

**Remediation of soils and groundwater**  
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**Problem set #1: contaminant properties**

Problem 1:

closed bottle            10 mL gas =  $10^{-5} \text{ m}^3 = V_G$   
                               90 mL water =  $9 \cdot 10^{-5} \text{ m}^3 = V_L$

$T = 20^\circ \text{C}$

$M_S = 36 \text{ mg}$  solid with specific gravity of 1

$$36 \cdot 10^{-3} \text{ g} \cdot \frac{1 \text{ cm}^3}{1 \text{ g}} \rightarrow V_s = 3.6 \cdot 10^{-8} \text{ m}^3$$

$f_{OC} = 0.1$

10 mg PCE

$MW_{PCE} = 166$

$K_H' = 0.6$

$\log K_{OW} = 2.67$

Mass balance:

$$m_{PCE,aq} + m_{PCE,g} + m_{PCE,s} = m_{PCE,t} = 10^{-2} \text{ g} \quad (1)$$

Partitioning coefficients:

$$K_H' \cdot \frac{V_G}{V_L} \cdot m_{PCE,aq} = m_{PCE,g} \quad (2)$$

$$\frac{K_D \cdot m_{PCE,aq} \cdot M_S}{V_L} = m_{PCE,s} \quad (3)$$

Calculating  $K_D$

$$\log K_{OC} = 0.989 \cdot \log K_{OW} - 0.346 = 2.29$$

$$K_D = f_{OC} \cdot K_{OC} = 19.7 \frac{\text{m}^3}{\text{g}}$$

Three equations and three unknowns:

From equation (1):

$$m_{PCE,aq} + \frac{K_H' \cdot V_G}{V_L} \cdot m_{PCE,aq} + \frac{K_D \cdot M_S}{V_L} \cdot m_{PCE,aq} = 10^{-2} \text{ g} = m_{PCE}$$

$$m_{PCE,aq} = \frac{10^{-2} \text{ g}}{\frac{0.6 \cdot 10^{-5} \text{ m}^3}{9 \cdot 10^{-5} \text{ m}^3} + \frac{19.7 \frac{\text{m}^3}{\text{g}} \cdot 36 \cdot 10^{-3} \text{ g}}{9 \cdot 10^{-5} \text{ m}^3} + 1} = \frac{10^{-2} \text{ g}}{0.0666 + 7880 + 1}$$

$$m_{PCE,aq} = 1.27 \cdot 10^{-6} \text{ g}$$

$$m_{PCE,s} = 7880 \cdot 1.27 \cdot 10^{-6} \text{ g} = 1.00 \cdot 10^{-2} \text{ g}$$

$$m_{PCE,g} = 0.0666 \cdot 5.6 \cdot 10^{-3} \text{ g} = 8.46 \cdot 10^{-8} \text{ g}$$

### Problem 2:

$$m_{\text{cont,total}} = m_{\text{cont,g}} + m_{\text{cont,aq}}$$

$$m_{\text{cont,total}} = C_{\text{cont,total}} V_L = C_{\text{cont,aq}} K_H' V_G + C_{\text{cont,aq}} V_L$$

$$C_{\text{cont,aq}} = \frac{C_{\text{cont,total}} \cdot V_L}{K_H' \cdot V_G + V_L}$$

$$C_{\text{benz,aq}} = 34.2 \mu\text{g/L}$$

$$C_{\text{tol,aq}} = 32.1 \mu\text{g/L}$$

$$C_{\text{ethylbenz,aq}} = 25.6 \mu\text{g/L}$$

$$C_{\text{xyl,aq}} = 26.2 \mu\text{g/L}$$

The actual concentration in the aqueous phase is much lower than the intended concentration. This solution needs to be stored with minimal headspace to minimize the volatilization of the compounds.

### Problem 3:

$$C_{\text{benz,s,initial}} = 900 \text{ mg/kg dry soil}$$

$$K_D = 0.02 \text{ m}^3/\text{kg}$$

$$\text{Solids concentration} = 40 \text{ kg dry soil/m}^3 \text{ slurry}$$

$$V_T = \text{volume of slurry} = 500 \text{ m}^3$$

$$\rho_s = 2,000 \text{ kg/m}^3$$

assume no headspace

a- What is  $V_L$ ?

$$M_s = \frac{40 \text{ kg}}{\text{m}^3 \text{ slurry}} \cdot 500 \text{ m}^3 \text{ slurry} = 20,000 \text{ kg soil}$$

$$V_s = 20,000 \text{ kg} \cdot \frac{1 \text{ m}^3}{2,000 \text{ kg}} = 10 \text{ m}^3$$

$$V_L = 490 \text{ m}^3$$

b - what is  $C_{\text{benz,aq}}$ ?

$$m_{\text{benz,total}} = m_{\text{benz,s}} + m_{\text{benz,aq}}$$

$$m_{\text{benz,total}} = C_{\text{benz,s,initial}} \cdot M_s = C_{\text{benz,s}} \cdot M_s + C_{\text{benz,aq}} \cdot V_L = C_{\text{benz,aq}} K_D M_s + C_{\text{benz,aq}} V_L$$

$$C_{\text{benz,aq}} = \frac{C_{\text{benz,initial}} \cdot M_s}{K_D \cdot M_s + V_L} = \frac{900 \frac{\text{mg}}{\text{kg}} \cdot 20,000 \text{ kg} \cdot \frac{1 \text{ g}}{10^3 \text{ mg}}}{0.02 \frac{\text{m}^3}{\text{kg}} \cdot 20,000 \text{ kg} + 490 \text{ m}^3} = 20.2 \frac{\text{g}}{\text{m}^3}$$

**Problem 4:**

**A – In a river**

$$C_{SS} = 10 \text{ mg/L}$$

$$K_{OW} = 10^6 \text{ (PCB)}$$

$$\rho_s = 1 \text{ g/cm}^3$$

$$f_{OC} = 0.1$$

What is the distribution of PCB between water and suspended solids?

$$K_D = \frac{C_{i,s}}{C_{i,aq}} \frac{[g/g]}{[g/m^3]} = 0.63 \cdot 10^{-6} \cdot f_{OC} \cdot K_{OW} = 6.3 \cdot 10^{-2} \frac{m^3}{g}$$

Fraction in the solid phase:

$$f_{PCB,s} = \frac{m_{PCB,s}}{m_{PCB,s} + m_{PCB,aq}} = \frac{\frac{m_{PCB,s}}{m_{PCB,aq}}}{\frac{m_{PCB,s}}{m_{PCB,aq}} + 1}$$

$$\begin{aligned} \frac{m_{PCB,s}}{m_{PCB,aq}} &= K_D \cdot C_{SS} = 6.3 \cdot 10^{-2} \frac{m^3}{g} \cdot \frac{10 \text{ mg}}{L} \cdot \frac{1'000 L}{1 m^3} \cdot \frac{1 g}{1'000 \text{ mg}} \\ &= 0.63 \frac{g \text{ PCB on solid}}{g \text{ PCB in solution}} \end{aligned}$$

$$f_{PCB,s} = \frac{0.63}{1.63} = 0.39$$

*Comment: over 1/3 of the PCB is on solids even if the solids represent 0.001 % of the total volume*

**B - For carbon tetrachloride CCl<sub>4</sub> (CT)**

$$K_{OW} = 440$$

$$\rho_s = 1.1 \text{ g/cm}^3$$

$$f_{OC} = 0.02$$

$$K_D = 0.63 \cdot 10^{-6} \cdot f_{OC} \cdot K_{OW} = 5.5 \cdot 10^{-6} \frac{m^3}{g}$$

Dimensionless partitioning coefficient:

$$K_p = \frac{C_{CT,s} \text{ in } \frac{g}{m^3}}{C_{CT,aq} \text{ in } \frac{g}{m^3}}$$

$$K_p = K_D \cdot \rho_s = 5.5 \cdot 10^{-6} \frac{m^3}{g} \cdot 1.1 \frac{g}{cm^3} \frac{10^6 cm^3}{m^3} = 6.1 [-]$$

**C - Mass distribution**

$V_S/V_T = 10^{-4}$ ; an approximation is that  $V_S/V_L \sim 10^{-4}$

$$\frac{m_{CT,s}}{m_{CT,aq}} = K_p \frac{V_S}{V_L} = 6.1 \cdot 10^{-4}$$

For CT, the distribution between solid and aqueous phase is very different as compared to PCBs. This is due to the difference in  $K_{OW}$ . PCBs have a high  $K_{OW}$  because they are hydrophobic and tend to associate with organic matter.