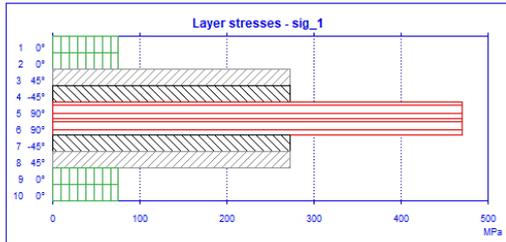


Par exemple : Lay-up de 10 plis de 0,45 et 90.
 Force Nx de 375000 N/m et Ny de 750000 N/m

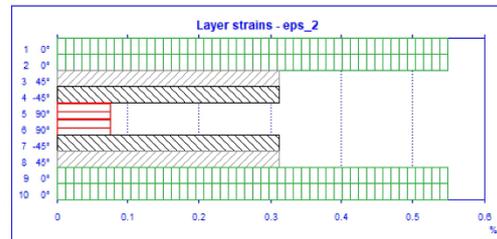
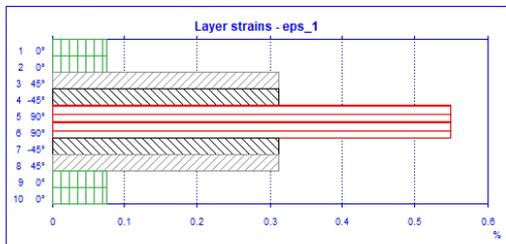
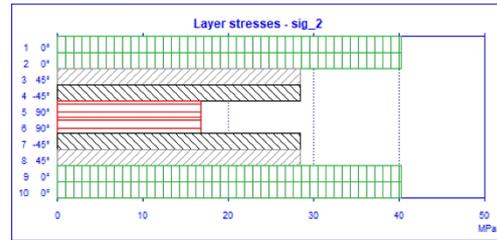
Contraintes et déformations dans chaque pli dans la direction des fibres et des forces.



Actual stress, Actual (=Eq.) strain



Actual stress, Actual (=Eq.) strain



Laminate : 04590G
 Modified : Mon Dec 16 18:07:27 2024

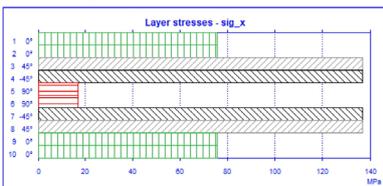
Lay-up : (0a/0a/+45a/-45a/90a/90a/-45a/+45a/0a/0a) h = 4.25 mm

Ply
 a T300,Epoxy,UD-.425/298/40

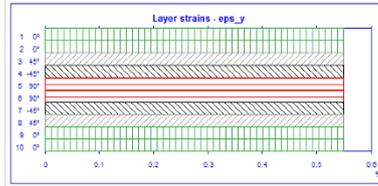
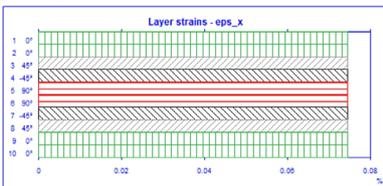
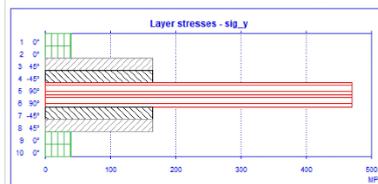
Load : Nx Ny
 Modified : Mon Dec 16 11:57:49 2024
 Type : Forces and moments (Var,E)

N_x = 375000 N/m M_x = 0 Nm/m
 N_y = 750000 N/m M_y = 0 Nm/m
 N_{xy} = 0 N/m M_{xy} = 0 Nm/m

Actual stress, Actual (=Eq.) strain



Actual stress, Actual (=Eq.) strain



Laminate : 04590G
 Modified : Mon Dec 16 18:07:27 2024

Lay-up : (0a/0a/+45a/-45a/90a/90a/-45a/+45a/0a/0a) h = 4.25 mm

Ply
 a T300,Epoxy,UD-.425/298/40

Load : Nx Ny
 Modified : Mon Dec 16 11:57:49 2024
 Type : Forces and moments (Var,E)

N_x = 375000 N/m M_x = 0 Nm/m
 N_y = 750000 N/m M_y = 0 Nm/m
 N_{xy} = 0 N/m M_{xy} = 0 Nm/m

Laminate : 04590G
 Modified : Mon Dec 16 18:07:27 2024

Lay-up : (0a/0a/+45a/-45a/90a/90a/-45a/+45a/0a/0a) h = 4.25 mm

Ply
 a T300,Epoxy,UD-.425/298/40

Load : Nx Ny
 Modified : Mon Dec 16 11:57:49 2024
 Type : Forces and moments (Var,E)

N_x = 375000 N/m M_x = 0 Nm/m
 N_y = 750000 N/m M_y = 0 Nm/m
 N_{xy} = 0 N/m M_{xy} = 0 Nm/m

RF pour 10 plis en UD epoxy/fibres de carbon T300

Ply: T300;Epoxy;UD-.425/298/40

Reinf.ply UD;Fiber;Carbon;Toray;Matrix;Epoxy;

t=0.42 mm;m_A=604 g/m²;rho=1420 kg/m³;V_f=40%;f_1/2=100/0;Transvis.23

Avec un FoSv de 1.

Avec un FoSv de 1.5

Laminate FPF analysis

Laminate : 04590C

Modified : Mon Dec 16 18:30:12 2024

Lay-up : (0a/0a/+45a/-45a/90a/90a/-45a/+45a/0a/0a) h = 4.25 mm

Ply

a T300;Epoxy;UD-.425/298/40

Load : Nx Ny

Modified : Mon Dec 16 11:57:49 2024

Type : Forces and moments (Var,E)

N_x = 375000 N/m M_x = 0 Nm/m
N_y = 750000 N/m M_y = 0 Nm/m
N_xy = 0 N/m M_xy = 0 Nm/m

Q_x = 0 N/m
Q_y = 0 N/m

Factor of safety : FoS_v = 1

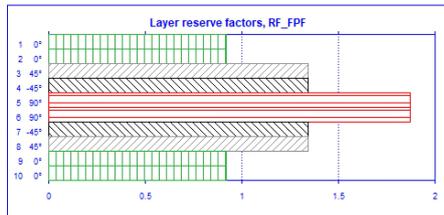
Failure criterion : Tsai-Wu; Max strain; Von Mises; Out-of-plane shear; Out-of-plane shear; None
(UD; non-UD; homogeneous; honeyc. core; foam/other core; adhesive)

Failure crit. param. : Tsai-Wu F₁₂²=0.5

Stress/strain recovery : layer top/bottom

Laminate margins of safety

| FPF | Mode | FPF-only | Mode | Crit. layers | ILS | Crit. interf. |
|----------|------|----------|------|--------------|-----|---------------|
| % | | % | | | % | |
| MoS = -8 | 2t | -8 | 2t | (0°) | - | - |



Laminate FPF analysis

Laminate : 04590C

Modified : Mon Dec 16 18:30:12 2024

Lay-up : (0a/0a/+45a/-45a/90a/90a/-45a/+45a/0a/0a) h = 4.25 mm

Ply

a T300;Epoxy;UD-.425/298/40

Load : Nx Ny

Modified : Mon Dec 16 11:57:49 2024

Type : Forces and moments (Var,E)

N_x = 375000 N/m M_x = 0 Nm/m
N_y = 750000 N/m M_y = 0 Nm/m
N_xy = 0 N/m M_xy = 0 Nm/m

Q_x = 0 N/m
Q_y = 0 N/m

Factor of safety : FoS_v = 1.5

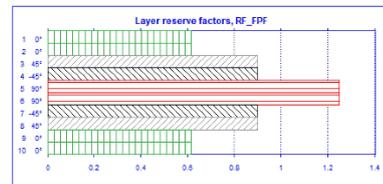
Failure criterion : Tsai-Wu; Max strain; Von Mises; Out-of-plane shear; Out-of-plane shear; None
(UD; non-UD; homogeneous; honeyc. core; foam/other core; adhesive)

Failure crit. param. : Tsai-Wu F₁₂²=0.5

Stress/strain recovery : layer top/bottom

Laminate margins of safety

| FPF | Mode | FPF-only | Mode | Crit. layers | ILS | Crit. interf. |
|-----------|------|----------|------|--------------|-----|---------------|
| % | | % | | | % | |
| MoS = -39 | 2t | -39 | 2t | (0°) | - | - |



FoS_v : factor of safety variable

RF = Frupture / Feffective = Frupture/(Fappliqué. FoSv)

Certains plis ont encore des RF inférieurs à 1.

RF pour 30 plis, avec des plis supplémentaires à 0
Les contraintes sig2 dans ces plis diminuent. Les RF deviennent supérieurs à 1.
L'épaisseur passe de 4.25 à 12.75 mm

$N_x = 375000 \text{ N/m}$ $M_x = 0 \text{ Nm/m}$
 $N_y = 750000 \text{ N/m}$ $M_y = 0 \text{ Nm/m}$
 $N_{xy} = 0 \text{ N/m}$ $M_{xy} = 0 \text{ Nm/m}$

Laminate stress-strain state

$Q_x = 0 \text{ N/m}$
 $Q_y = 0 \text{ N/m}$

Laminate : **04590C 30p**

Modified : Fri Dec 20 14:36:14 2024

Lay-up :- h = 12.75 mm

Ply
a T300,Epoxy;UD-.425/298/40

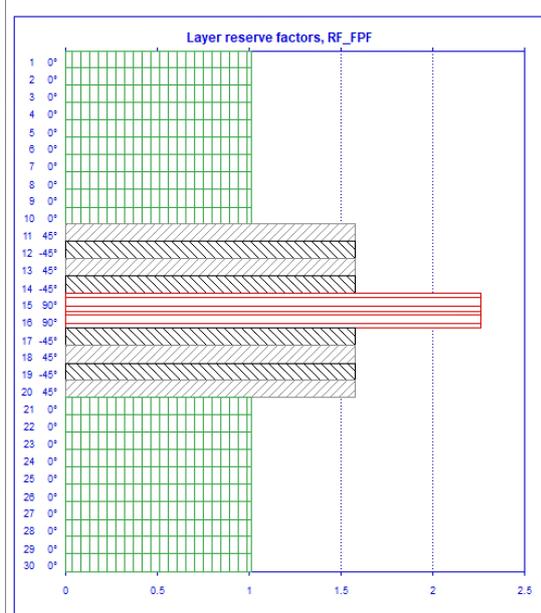
Load : **Nx Ny**

Modified : Mon Dec 16 11:57:49 2024

Type : Forces and moments (Var;E)

$N_x = 375000 \text{ N/m}$ $M_x = 0 \text{ Nm/m}$
 $N_y = 750000 \text{ N/m}$ $M_y = 0 \text{ Nm/m}$
 $N_{xy} = 0 \text{ N/m}$ $M_{xy} = 0 \text{ Nm/m}$

| Ply | theta | sig_1 | sig_2 | tau_12 | tau_31 | tau_23 | sig_x | sig_y | tau_xy | tau_xz | tau_yz |
|-----|---------|--------|-------|--------|--------|--------|-------|--------|--------|--------|--------|
| | ° | MPa | MPa | MPa | MPa | MPa | MPa | MPa | MPa | MPa | MPa |
| 1 | a 0 t | 14.44 | 23.41 | 0.00 | 0.00 | 0.00 | 14.44 | 23.41 | 0.00 | 0.00 | 0.00 |
| | b | 14.44 | 23.41 | 0.00 | 0.00 | 0.00 | 14.44 | 23.41 | 0.00 | 0.00 | 0.00 |
| 2 | a 0 t | 14.44 | 23.41 | 0.00 | 0.00 | 0.00 | 14.44 | 23.41 | 0.00 | 0.00 | 0.00 |
| | b | 14.44 | 23.41 | 0.00 | 0.00 | 0.00 | 14.44 | 23.41 | 0.00 | 0.00 | 0.00 |
| 3 | a 0 t | 14.44 | 23.41 | 0.00 | 0.00 | 0.00 | 14.44 | 23.41 | 0.00 | 0.00 | 0.00 |
| | b | 14.44 | 23.41 | 0.00 | 0.00 | 0.00 | 14.44 | 23.41 | 0.00 | 0.00 | 0.00 |
| 4 | a 0 t | 14.44 | 23.41 | 0.00 | 0.00 | 0.00 | 14.44 | 23.41 | 0.00 | 0.00 | 0.00 |
| | b | 14.44 | 23.41 | 0.00 | 0.00 | 0.00 | 14.44 | 23.41 | 0.00 | 0.00 | 0.00 |
| 5 | a 0 t | 14.44 | 23.41 | 0.00 | 0.00 | 0.00 | 14.44 | 23.41 | 0.00 | 0.00 | 0.00 |
| | b | 14.44 | 23.41 | 0.00 | 0.00 | 0.00 | 14.44 | 23.41 | 0.00 | 0.00 | 0.00 |
| 6 | a 0 t | 14.44 | 23.41 | 0.00 | 0.00 | 0.00 | 14.44 | 23.41 | 0.00 | 0.00 | 0.00 |
| | b | 14.44 | 23.41 | 0.00 | 0.00 | 0.00 | 14.44 | 23.41 | 0.00 | 0.00 | 0.00 |
| 7 | a 0 t | 14.44 | 23.41 | 0.00 | 0.00 | 0.00 | 14.44 | 23.41 | 0.00 | 0.00 | 0.00 |
| | b | 14.44 | 23.41 | 0.00 | 0.00 | 0.00 | 14.44 | 23.41 | 0.00 | 0.00 | 0.00 |
| 8 | a 0 t | 14.44 | 23.41 | 0.00 | 0.00 | 0.00 | 14.44 | 23.41 | 0.00 | 0.00 | 0.00 |
| | b | 14.44 | 23.41 | 0.00 | 0.00 | 0.00 | 14.44 | 23.41 | 0.00 | 0.00 | 0.00 |
| 9 | a 0 t | 14.44 | 23.41 | 0.00 | 0.00 | 0.00 | 14.44 | 23.41 | 0.00 | 0.00 | 0.00 |
| | b | 14.44 | 23.41 | 0.00 | 0.00 | 0.00 | 14.44 | 23.41 | 0.00 | 0.00 | 0.00 |
| 10 | a 0 t | 14.44 | 23.41 | 0.00 | 0.00 | 0.00 | 14.44 | 23.41 | 0.00 | 0.00 | 0.00 |
| | b | 14.44 | 23.41 | 0.00 | 0.00 | 0.00 | 14.44 | 23.41 | 0.00 | 0.00 | 0.00 |
| 11 | a 45 t | 148.31 | 15.50 | 9.62 | 0.00 | 0.00 | 72.29 | 91.52 | 66.41 | 0.00 | 0.00 |
| | b | 148.31 | 15.50 | 9.62 | 0.00 | 0.00 | 72.29 | 91.52 | 66.41 | 0.00 | 0.00 |
| 12 | a -45 t | 148.31 | 15.50 | -9.62 | 0.00 | 0.00 | 72.29 | 91.52 | -66.41 | 0.00 | 0.00 |
| | b | 148.31 | 15.50 | -9.62 | 0.00 | 0.00 | 72.29 | 91.52 | -66.41 | 0.00 | 0.00 |
| 13 | a 45 t | 148.31 | 15.50 | 9.62 | 0.00 | 0.00 | 72.29 | 91.52 | 66.41 | 0.00 | 0.00 |
| | b | 148.31 | 15.50 | 9.62 | 0.00 | 0.00 | 72.29 | 91.52 | 66.41 | 0.00 | 0.00 |
| 14 | a -45 t | 148.31 | 15.50 | -9.62 | 0.00 | 0.00 | 72.29 | 91.52 | -66.41 | 0.00 | 0.00 |
| | b | 148.31 | 15.50 | -9.62 | 0.00 | 0.00 | 72.29 | 91.52 | -66.41 | 0.00 | 0.00 |
| 15 | a 90 t | 282.18 | 7.58 | 0.00 | 0.00 | 0.00 | 7.58 | 282.18 | 0.00 | 0.00 | 0.00 |
| | b | 282.18 | 7.58 | 0.00 | 0.00 | 0.00 | 7.58 | 282.18 | 0.00 | 0.00 | 0.00 |
| 16 | a 90 t | 282.18 | 7.58 | 0.00 | 0.00 | 0.00 | 7.58 | 282.18 | 0.00 | 0.00 | 0.00 |
| | b | 282.18 | 7.58 | 0.00 | 0.00 | 0.00 | 7.58 | 282.18 | 0.00 | 0.00 | 0.00 |
| 17 | a -45 t | 148.31 | 15.50 | -9.62 | 0.00 | 0.00 | 72.29 | 91.52 | -66.41 | 0.00 | 0.00 |
| | b | 148.31 | 15.50 | -9.62 | 0.00 | 0.00 | 72.29 | 91.52 | -66.41 | 0.00 | 0.00 |
| 18 | a 45 t | 148.31 | 15.50 | 9.62 | 0.00 | 0.00 | 72.29 | 91.52 | 66.41 | 0.00 | 0.00 |
| | b | 148.31 | 15.50 | 9.62 | 0.00 | 0.00 | 72.29 | 91.52 | 66.41 | 0.00 | 0.00 |
| 19 | a -45 t | 148.31 | 15.50 | -9.62 | 0.00 | 0.00 | 72.29 | 91.52 | -66.41 | 0.00 | 0.00 |
| | b | 148.31 | 15.50 | -9.62 | 0.00 | 0.00 | 72.29 | 91.52 | -66.41 | 0.00 | 0.00 |
| 20 | a 45 t | 148.31 | 15.50 | 9.62 | 0.00 | 0.00 | 72.29 | 91.52 | 66.41 | 0.00 | 0.00 |
| | b | 148.31 | 15.50 | 9.62 | 0.00 | 0.00 | 72.29 | 91.52 | 66.41 | 0.00 | 0.00 |
| 21 | a 0 t | 14.44 | 23.41 | 0.00 | 0.00 | 0.00 | 14.44 | 23.41 | 0.00 | 0.00 | 0.00 |
| | b | 14.44 | 23.41 | 0.00 | 0.00 | 0.00 | 14.44 | 23.41 | 0.00 | 0.00 | 0.00 |



16 plis avec une autre répartition des contraintes, plus de plis à 90 où les fibres reprennent plus les contraintes radiales. Ainsi les contraintes sigma2 sur les 4 plis à 0 sont diminuées et leur RF devient supérieur à 1. L'épaisseur et donc le poids du composite sont plus petits que le stratifié à 30 plis.

Laminate FPF analysis

Laminate : 04590C

Modified : Fri Dec 20 14:53:41 2024

Lay-up : (0a/0a/+45a/-45a/+45a/-45a/90a/90a/90a/90a/-45a/+45a/-45a/+45a/0a/0a) h = 6.8 mm

Ply

a T300/Epoxy/UD-42529040

Load : Nx Ny

Modified : Mon Dec 16 11:57:49 2024

Type : Forces and moments (Var,E)

N_x = 375000 N/m M_x = 0 Nmm
 N_y = 750000 N/m M_y = 0 Nmm
 N_{xy} = 0 N/m M_{xy} = 0 Nmm

Q_x = 0 N/m
 Q_y = 0 N/m

Factor of safety: FoS^v = 1.5

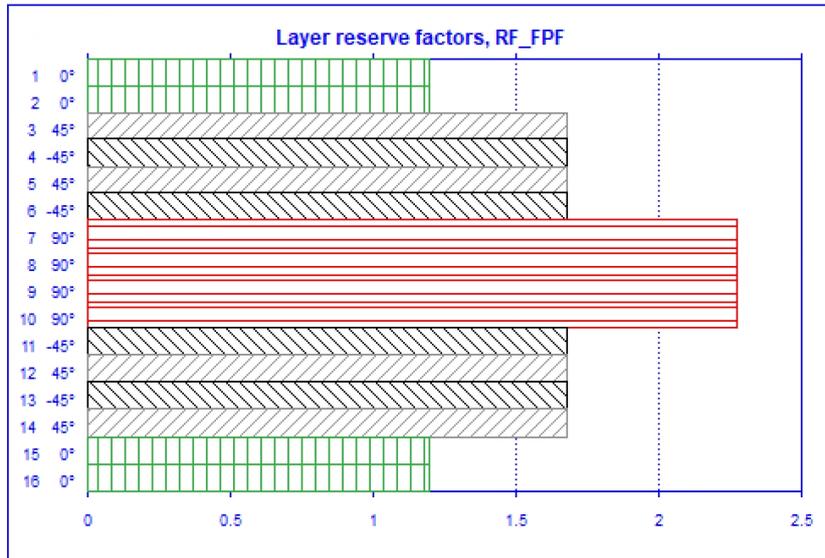
Failure criterion : Tsai-Wu, Tsai-Wu, Von Mises, Out-of-plane shear, Out-of-plane shear, None

(UD, non-UD; homogeneous; honeyc; core; foam/other core; adhesive)

Failure crit. param.: Tsai-Wu F₁₂^v = -0.5

Stress/strain recovery : layer top/bottom

| Ply | theta | * | sig_1 | sig_2 | tau_12 | tau_31 | tau_23 | sig_x | sig_y | tau_xy | tau_zx | tau_yz |
|-----|-------|-----|-------|--------|--------|--------|--------|-------|-------|--------|--------|--------|
| | | | MPa | MPa | MPa | MPa | MPa | MPa | MPa | MPa | MPa | MPa |
| 1 | a | 0 | t | 58.09 | 21.07 | 0.00 | 0.00 | 0.00 | 58.09 | 21.07 | 0.00 | 0.00 |
| | | | b | 58.09 | 21.07 | 0.00 | 0.00 | 0.00 | 58.09 | 21.07 | 0.00 | 0.00 |
| 2 | a | 0 | t | 58.09 | 21.07 | 0.00 | 0.00 | 0.00 | 58.09 | 21.07 | 0.00 | 0.00 |
| | | | b | 58.09 | 21.07 | 0.00 | 0.00 | 0.00 | 58.09 | 21.07 | 0.00 | 0.00 |
| 3 | a | 45 | t | 149.79 | 15.65 | 6.59 | 0.00 | 0.00 | 76.13 | 89.31 | 67.07 | 0.00 |
| | | | b | 149.79 | 15.65 | 6.59 | 0.00 | 0.00 | 76.13 | 89.31 | 67.07 | 0.00 |
| 4 | a | -45 | t | 149.79 | 15.65 | -6.59 | 0.00 | 0.00 | 76.13 | 89.31 | -67.07 | 0.00 |
| | | | b | 149.79 | 15.65 | -6.59 | 0.00 | 0.00 | 76.13 | 89.31 | -67.07 | 0.00 |
| 5 | a | 45 | t | 149.79 | 15.65 | 6.59 | 0.00 | 0.00 | 76.13 | 89.31 | 67.07 | 0.00 |
| | | | b | 149.79 | 15.65 | 6.59 | 0.00 | 0.00 | 76.13 | 89.31 | 67.07 | 0.00 |
| 6 | a | -45 | t | 149.79 | 15.65 | -6.59 | 0.00 | 0.00 | 76.13 | 89.31 | -67.07 | 0.00 |
| | | | b | 149.79 | 15.65 | -6.59 | 0.00 | 0.00 | 76.13 | 89.31 | -67.07 | 0.00 |
| 7 | a | 90 | t | 241.49 | 10.23 | 0.00 | 0.00 | 0.00 | 10.23 | 241.49 | 0.00 | 0.00 |
| | | | b | 241.49 | 10.23 | 0.00 | 0.00 | 0.00 | 10.23 | 241.49 | 0.00 | 0.00 |
| 8 | a | 90 | t | 241.49 | 10.23 | 0.00 | 0.00 | 0.00 | 10.23 | 241.49 | 0.00 | 0.00 |
| | | | b | 241.49 | 10.23 | 0.00 | 0.00 | 0.00 | 10.23 | 241.49 | 0.00 | 0.00 |
| 9 | a | 90 | t | 241.49 | 10.23 | 0.00 | 0.00 | 0.00 | 10.23 | 241.49 | 0.00 | 0.00 |
| | | | b | 241.49 | 10.23 | 0.00 | 0.00 | 0.00 | 10.23 | 241.49 | 0.00 | 0.00 |
| 10 | a | 90 | t | 241.49 | 10.23 | 0.00 | 0.00 | 0.00 | 10.23 | 241.49 | 0.00 | 0.00 |
| | | | b | 241.49 | 10.23 | 0.00 | 0.00 | 0.00 | 10.23 | 241.49 | 0.00 | 0.00 |
| 11 | a | -45 | t | 149.79 | 15.65 | -6.59 | 0.00 | 0.00 | 76.13 | 89.31 | -67.07 | 0.00 |
| | | | b | 149.79 | 15.65 | -6.59 | 0.00 | 0.00 | 76.13 | 89.31 | -67.07 | 0.00 |
| 12 | a | 45 | t | 149.79 | 15.65 | 6.59 | 0.00 | 0.00 | 76.13 | 89.31 | 67.07 | 0.00 |
| | | | b | 149.79 | 15.65 | 6.59 | 0.00 | 0.00 | 76.13 | 89.31 | 67.07 | 0.00 |
| 13 | a | -45 | t | 149.79 | 15.65 | -6.59 | 0.00 | 0.00 | 76.13 | 89.31 | -67.07 | 0.00 |
| | | | b | 149.79 | 15.65 | -6.59 | 0.00 | 0.00 | 76.13 | 89.31 | -67.07 | 0.00 |
| 14 | a | 45 | t | 149.79 | 15.65 | 6.59 | 0.00 | 0.00 | 76.13 | 89.31 | 67.07 | 0.00 |
| | | | b | 149.79 | 15.65 | 6.59 | 0.00 | 0.00 | 76.13 | 89.31 | 67.07 | 0.00 |
| 15 | a | 0 | t | 58.09 | 21.07 | 0.00 | 0.00 | 0.00 | 58.09 | 21.07 | 0.00 | 0.00 |
| | | | b | 58.09 | 21.07 | 0.00 | 0.00 | 0.00 | 58.09 | 21.07 | 0.00 | 0.00 |
| 16 | a | 0 | t | 58.09 | 21.07 | 0.00 | 0.00 | 0.00 | 58.09 | 21.07 | 0.00 | 0.00 |
| | | | b | 58.09 | 21.07 | 0.00 | 0.00 | 0.00 | 58.09 | 21.07 | 0.00 | 0.00 |



18 plis dont 2 plis externes en Kevlar pour la résistance aux chocs.

Layer stresses

Laminate : **04590 CK**

Modified : Fri Dec 20 15:17:21 2024

Lay-up : (0a/0b/0b/+45b/-45b/+45b/-45b/90b/90b/90b/90b/-45b/+45b/-45b/+45b/0b/0b/0a) h = 7.2 mm

Ply

- a Kevlar 49;Epoxy;UD-.200/173/60
- b T300;Epoxy;UD-.425/298/40

Load : **Nx Ny**

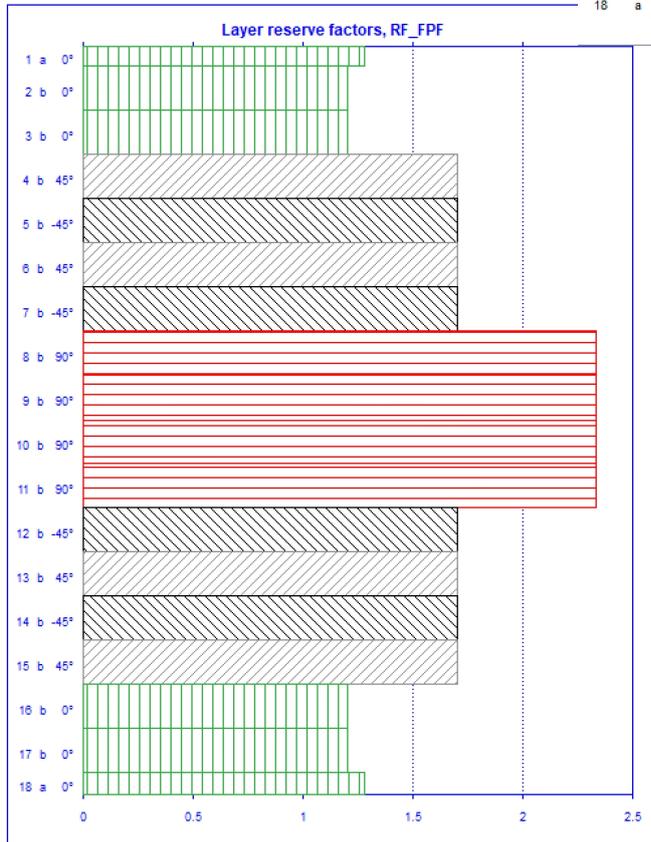
Modified : Mon Dec 16 11:57:49 2024

Type : Forces and moments (Var.;E)

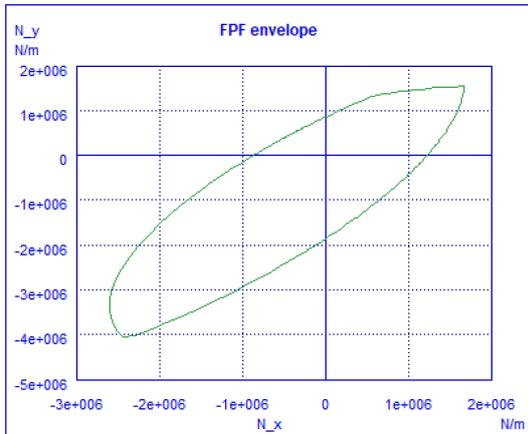
$N_x = 375000 \text{ N/m}$ $M_x = 0 \text{ Nm/m}$
 $N_y = 750000 \text{ N/m}$ $M_y = 0 \text{ Nm/m}$
 $N_{xy} = 0 \text{ N/m}$ $M_{xy} = 0 \text{ Nm/m}$

$Q_x = 0 \text{ N/m}$
 $Q_y = 0 \text{ N/m}$

| Ply | theta | | sig_1 MPa | sig_2 MPa | tau_12 MPa | tau_31 MPa | tau_23 MPa | sig_x MPa | sig_y MPa | tau_xy MPa | tau_xz MPa | tau_yz MPa |
|-----|-------|-----|--------------|--------------|---------------|---------------|---------------|--------------|--------------|---------------|---------------|---------------|
| 1 | a | 0 | t | 45.89 | 16.55 | 0.00 | 0.00 | 0.00 | 45.89 | 16.55 | 0.00 | 0.00 |
| | | | b | 45.89 | 16.55 | 0.00 | 0.00 | 0.00 | 45.89 | 16.55 | 0.00 | 0.00 |
| 2 | b | 0 | t | 51.90 | 20.89 | 0.00 | 0.00 | 0.00 | 51.90 | 20.89 | 0.00 | 0.00 |
| | | | b | 51.90 | 20.89 | 0.00 | 0.00 | 0.00 | 51.90 | 20.89 | 0.00 | 0.00 |
| 3 | b | 0 | t | 51.90 | 20.89 | 0.00 | 0.00 | 0.00 | 51.90 | 20.89 | 0.00 | 0.00 |
| | | | b | 51.90 | 20.89 | 0.00 | 0.00 | 0.00 | 51.90 | 20.89 | 0.00 | 0.00 |
| 4 | b | 45 | t | 146.47 | 15.30 | 6.79 | 0.00 | 0.00 | 74.09 | 87.68 | 65.58 | 0.00 |
| | | | b | 146.47 | 15.30 | 6.79 | 0.00 | 0.00 | 74.09 | 87.68 | 65.58 | 0.00 |
| 5 | b | -45 | t | 146.47 | 15.30 | -6.79 | 0.00 | 0.00 | 74.09 | 87.68 | -65.58 | 0.00 |
| | | | b | 146.47 | 15.30 | -6.79 | 0.00 | 0.00 | 74.09 | 87.68 | -65.58 | 0.00 |
| 6 | b | 45 | t | 146.47 | 15.30 | 6.79 | 0.00 | 0.00 | 74.09 | 87.68 | 65.58 | 0.00 |
| | | | b | 146.47 | 15.30 | 6.79 | 0.00 | 0.00 | 74.09 | 87.68 | 65.58 | 0.00 |
| 7 | b | -45 | t | 146.47 | 15.30 | -6.79 | 0.00 | 0.00 | 74.09 | 87.68 | -65.58 | 0.00 |
| | | | b | 146.47 | 15.30 | -6.79 | 0.00 | 0.00 | 74.09 | 87.68 | -65.58 | 0.00 |
| 8 | b | 90 | t | 241.03 | 9.71 | 0.00 | 0.00 | 0.00 | 9.71 | 241.03 | 0.00 | 0.00 |
| | | | b | 241.03 | 9.71 | 0.00 | 0.00 | 0.00 | 9.71 | 241.03 | 0.00 | 0.00 |
| 9 | b | 90 | t | 241.03 | 9.71 | 0.00 | 0.00 | 0.00 | 9.71 | 241.03 | 0.00 | 0.00 |
| | | | b | 241.03 | 9.71 | 0.00 | 0.00 | 0.00 | 9.71 | 241.03 | 0.00 | 0.00 |
| 10 | b | 90 | t | 241.03 | 9.71 | 0.00 | 0.00 | 0.00 | 9.71 | 241.03 | 0.00 | 0.00 |
| | | | b | 241.03 | 9.71 | 0.00 | 0.00 | 0.00 | 9.71 | 241.03 | 0.00 | 0.00 |
| 11 | b | 90 | t | 241.03 | 9.71 | 0.00 | 0.00 | 0.00 | 9.71 | 241.03 | 0.00 | 0.00 |
| | | | b | 241.03 | 9.71 | 0.00 | 0.00 | 0.00 | 9.71 | 241.03 | 0.00 | 0.00 |
| 12 | b | -45 | t | 146.47 | 15.30 | -6.79 | 0.00 | 0.00 | 74.09 | 87.68 | -65.58 | 0.00 |
| | | | b | 146.47 | 15.30 | -6.79 | 0.00 | 0.00 | 74.09 | 87.68 | -65.58 | 0.00 |
| 13 | b | 45 | t | 146.47 | 15.30 | 6.79 | 0.00 | 0.00 | 74.09 | 87.68 | 65.58 | 0.00 |
| | | | b | 146.47 | 15.30 | 6.79 | 0.00 | 0.00 | 74.09 | 87.68 | 65.58 | 0.00 |
| 14 | b | -45 | t | 146.47 | 15.30 | -6.79 | 0.00 | 0.00 | 74.09 | 87.68 | -65.58 | 0.00 |
| | | | b | 146.47 | 15.30 | -6.79 | 0.00 | 0.00 | 74.09 | 87.68 | -65.58 | 0.00 |
| 15 | b | 45 | t | 146.47 | 15.30 | 6.79 | 0.00 | 0.00 | 74.09 | 87.68 | 65.58 | 0.00 |
| | | | b | 146.47 | 15.30 | 6.79 | 0.00 | 0.00 | 74.09 | 87.68 | 65.58 | 0.00 |
| 16 | b | 0 | t | 51.90 | 20.89 | 0.00 | 0.00 | 0.00 | 51.90 | 20.89 | 0.00 | 0.00 |
| | | | b | 51.90 | 20.89 | 0.00 | 0.00 | 0.00 | 51.90 | 20.89 | 0.00 | 0.00 |
| 17 | b | 0 | t | 51.90 | 20.89 | 0.00 | 0.00 | 0.00 | 51.90 | 20.89 | 0.00 | 0.00 |
| | | | b | 51.90 | 20.89 | 0.00 | 0.00 | 0.00 | 51.90 | 20.89 | 0.00 | 0.00 |
| 18 | a | 0 | t | 45.89 | 16.55 | 0.00 | 0.00 | 0.00 | 45.89 | 16.55 | 0.00 | 0.00 |
| | | | b | 45.89 | 16.55 | 0.00 | 0.00 | 0.00 | 45.89 | 16.55 | 0.00 | 0.00 |



Enveloppe de rupture



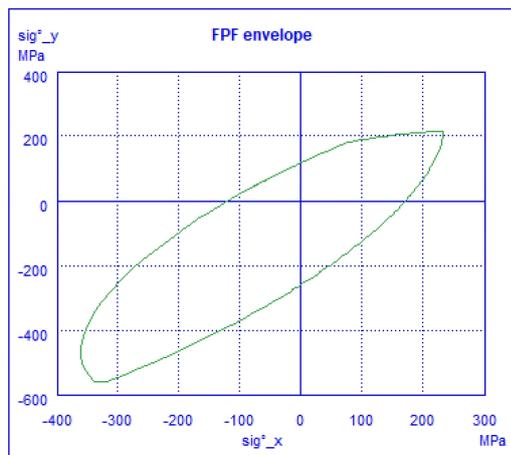
Plot x- and y-components not in the same scale.

Failure criterion : Tsai-Wu; Tsai-Wu; Von Mises; Out-of-plane shear; Out-of-plane shear; None
 (UD; non-UD; homogeneous; honeyc. core; foam/other core; adhesive)
 Failure crit. param. : Tsai-Wu $F_{12}^* = -0.5$
 Stress/strain recovery : layer top/bottom

Laminate : **04590 CK**
 Modified : Fri Dec 20 15:17:21 2024

Lay-up : (0a/0b/0b/+45b/-45b/+45b/-45b/90b/90b/90b/90b/-45b/+45b/-45b/+45b/0b/0b/0a) h = 7.2 mm

Ply
 a Kevlar 49;Epoxy;UD-.200/173/60
 b T300;Epoxy;UD-.425/298/40



Plot x- and y-components not in the same scale.

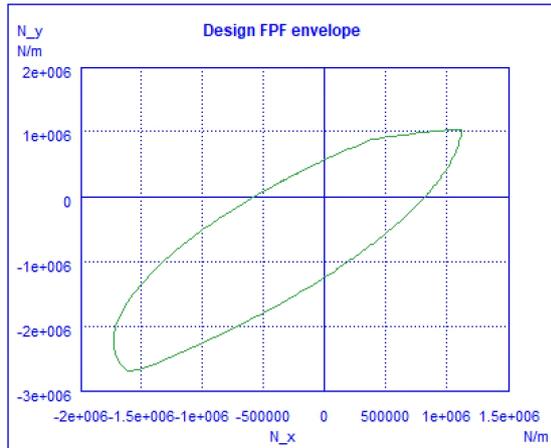
Failure criterion : Tsai-Wu; Tsai-Wu; Von Mises; Out-of-plane shear; Out-of-plane shear; None
 (UD; non-UD; homogeneous; honeyc. core; foam/other core; adhesive)
 Failure crit. param. : Tsai-Wu $F_{12}^* = -0.5$
 Stress/strain recovery : layer top/bottom

Laminate : **04590 CK**
 Modified : Fri Dec 20 15:17:21 2024

Lay-up : (0a/0b/0b/+45b/-45b/+45b/-45b/90b/90b/90b/90b/-45b/+45b/-45b/+45b/0b/0b/0a) h = 7.2 mm

Ply
 a Kevlar 49;Epoxy;UD-.200/173/60
 b T300;Epoxy;UD-.425/298/40

Enveloppe de rupture avec FoS_v de 1.5.

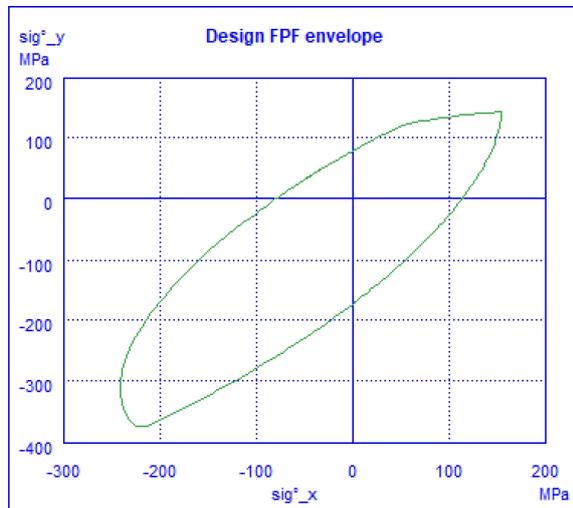


Factor of safety : $FoS^v = 1.5$
 Failure criterion : Tsai-Wu; Tsai-Wu; Von Mises; Out-of-plane shear; Out-of-plane shear; None
 (UD; non-UD; homogeneous; honeyc. core; foam/other core; adhesive)
 Failure crit. param. : Tsai-Wu $F_{12}^* = -0.5$
 Stress/strain recovery : layer top/bottom

Laminate : **04590 CK**
 Modified : Fri Dec 20 15:17:21 2024

Lay-up : (0a/0b/0b/+45b/-45b/+45b/-45b/90b/90b/90b/90b/-45b/+45b/-45b/+45b/0b/0b/0a) h = 7.2 mm

Ply
 a Kevlar 49;Epoxy;UD-.200/173/60
 b T300;Epoxy;UD-.425/298/40



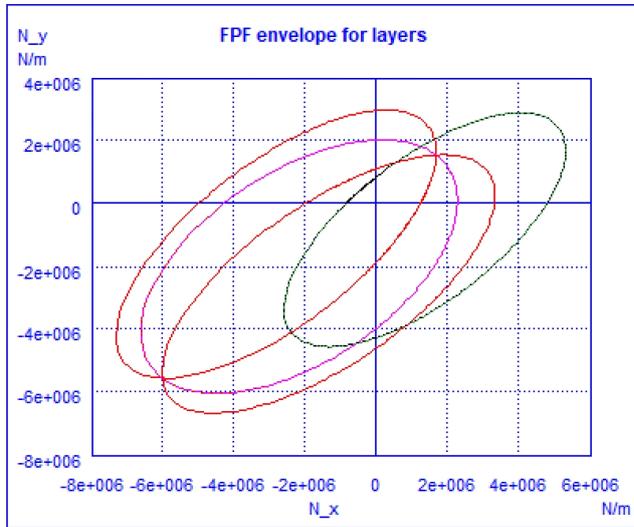
Factor of safety : $FoS^v = 1.5$
 Failure criterion : Tsai-Wu; Tsai-Wu; Von Mises; Out-of-plane shear; Out-of-plane shear; None
 (UD; non-UD; homogeneous; honeyc. core; foam/other core; adhesive)
 Failure crit. param. : Tsai-Wu $F_{12}^* = -0.5$
 Stress/strain recovery : layer top/bottom

Laminate : **04590 CK**
 Modified : Fri Dec 20 15:17:21 2024

Lay-up : (0a/0b/0b/+45b/-45b/+45b/-45b/90b/90b/90b/90b/-45b/+45b/-45b/+45b/0b/0b/0a) h = 7.2 mm

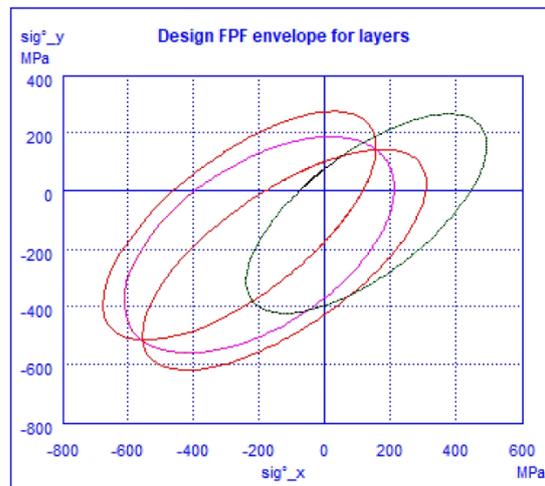
Ply
 a Kevlar 49;Epoxy;UD-.200/173/60
 b T300;Epoxy;UD-.425/298/40

Enveloppes de rupture pour chacun des plis.



- 1 a 0°
- 2 b 0°
- 3 b 0°
- 4 b 45°
- 5 b -45°
- 6 b 45°
- 7 b -45°
- 8 b 90°
- 9 b 90°
- 10 b 90°
- 11 b 90°
- 12 b -45°
- 13 b 45°
- 14 b -45°
- 15 b 45°
- 16 b 0°
- 17 b 0°
- 18 a 0°

Plot x- and y-components not in the same scale.



- 1 a 0°
- 2 b 0°
- 3 b 0°
- 4 b 45°
- 5 b -45°
- 6 b 45°
- 7 b -45°
- 8 b 90°
- 9 b 90°
- 10 b 90°
- 11 b 90°
- 12 b -45°
- 13 b 45°
- 14 b -45°
- 15 b 45°
- 16 b 0°
- 17 b 0°
- 18 a 0°

Plot x- and y-components not in the same scale.

Factor of safety : FoS^v = 1.5

Failure criterion : Tsai-Wu; Tsai-Wu; Von Mises; Out-of-plane shear; Out-of-plane shear; None (UD; non-UD; homogeneous; honeyc. core; foam/other core; adhesive)

Failure crit. param. : Tsai-Wu F₁₂* = -0.5

Stress/strain recovery : layer top/bottom

Laminate : 04590 CK

Modified : Fri Dec 20 15:17:21 2024