# Nuclear Fusion and Plasma Physics - Exercises 

Prof. A. Fasoli - Swiss Plasma Center / EPFL

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## Exercise 1 - A steady state Tokamak with copper coils

a) Using Ampere's law on a contour following the magnetic axis of the tokamak yields $2 \pi R B_{0}=\mu_{0} I_{\mathrm{enc}}$ so $I_{\mathrm{enc}}=150 \mathrm{MA}$. Dividing this result by 20 coils gives $7.5 \mathrm{MA} /$ coil.
b) The cross section is $S=I_{\text {coil }} / j_{c d}=0.15 \mathrm{~m}^{2}$. Assuming a circular coil its circumference is $\ell=2 \pi a=12.6 \mathrm{~m}$. The resistance of the coil is $R=\rho \ell / S=1.4 \times 10^{-6} \Omega$. This gives a power loss of 79 MW .
c) The resistivity is now reduced to $2 \times 10^{-9} \Omega \mathrm{~m}$. This gives a resistance $R=1.67 \times$ $10^{-7} \Omega$. The power loss now is 9.4 MW .

## Exercise 2-Design of a SC solenoid

This exercise is based on Section 3.1 of the book "Superconducting magnets" by M. Wilson. This solution follows closely the discussion in the book.
a) For a 6 T magnet, Fig. 5 in the problemset shows a critical current density $J \approx$ $3 \times 10^{8} \mathrm{Am}^{-2}$ (point Q in Fig. 5a).
b) Since $2 a=150 \mathrm{~mm}$, we use the result in (a) to find $F$ :

$$
F(\alpha, \beta)=\frac{B}{a J}=\frac{6 \mathrm{~T}}{0.075 \mathrm{~m} \cdot 3 \times 10^{8} \mathrm{Am}^{-2}}=2.7 \times 10^{-7} \mathrm{H} \mathrm{~m}^{-1}
$$

Then, using Fig. 3, we find the $\alpha$ and $\beta$ corresponding to the minimum volume for this value of $F$. We do this by, first, estimating by eye the curve for $F=2.7 \times 10^{-7} \mathrm{Hm}^{-1}$ between $2 \times 10^{-7} \mathrm{H} \mathrm{m}^{-1}$ and $3 \times 10^{-7} \mathrm{H} \mathrm{m}^{-1}$. Then, we think about the place where this curve would intersect the min_volume line. This happens approximately at $(\alpha, \beta)=$ $(1.4,0.7)$.
c) Figure 4 shows $B_{\mathrm{w}} / B_{0}=1.3$ for the parameter values obtained in (b).
d) If we want the magnet to produce $B_{0}=6 \mathrm{~T}$, the result above tells us that $B_{\mathrm{w}}=$ $1.3 \cdot 6 \mathrm{~T}=7.8 \mathrm{~T}$.
Looking at Fig. 5a, this means that running the design current of $J=3 \times 10^{8} \mathrm{Am}^{-2}$ would actually bring us to point $S$, which is beyond the limit of what the superconductor can take.
In order to stay within operational limits, we need to go back to point R (still referring to Fig. 5a), that is, we need to reduce the current density to $J=2.5 \times 10^{8} \mathrm{Am}^{-2}$ for a maximum field $B_{\mathrm{w}} \approx 6.5 \mathrm{~T}$.
Sadly enough, in that case our design would yield $B_{0}=B_{\mathrm{w}} / 1.3 \approx 5 \mathrm{~T}$.
e) To be able to achieve $B_{0}=6 \mathrm{~T}$, we need the design to allow for the higher value of $B_{\mathrm{w}}$, as shown in Fig. 5b.

If we choose $J=2 \times 10^{8} \mathrm{Am}^{-2}$ and $B=7.5 \mathrm{~T}$, then $F=5 \times 10^{-7} \mathrm{Hm}^{-1}$. The minimum volume is achieved with $(\alpha, \beta)=(1.7,0.9)$, which yields $B_{\mathrm{w}} / B_{0}=1.2$.
$B_{0}$ can now be as large as $B_{0}=7.5 / 1.2 \mathrm{~T}=6.25 \mathrm{~T}$.
This design is able to reach magnetic fields that are higher than the design goal, which may be undesirable (one can anyway always reduce $B_{0}$ by using a smaller $J$ ) since a larger magnet may be more expensive. One can continue iterating with values not far from these to find the parameters that exactly meet the requirement of $B_{0}$ ( $F=4 \times 10^{-7} \mathrm{H} \mathrm{m}^{-1}$ ).

One can also take a more efficient design by moving away from the minimum volume curve. For example, one can obtain more uniform field lines or achieve less winding volume with a longer magnet.

