

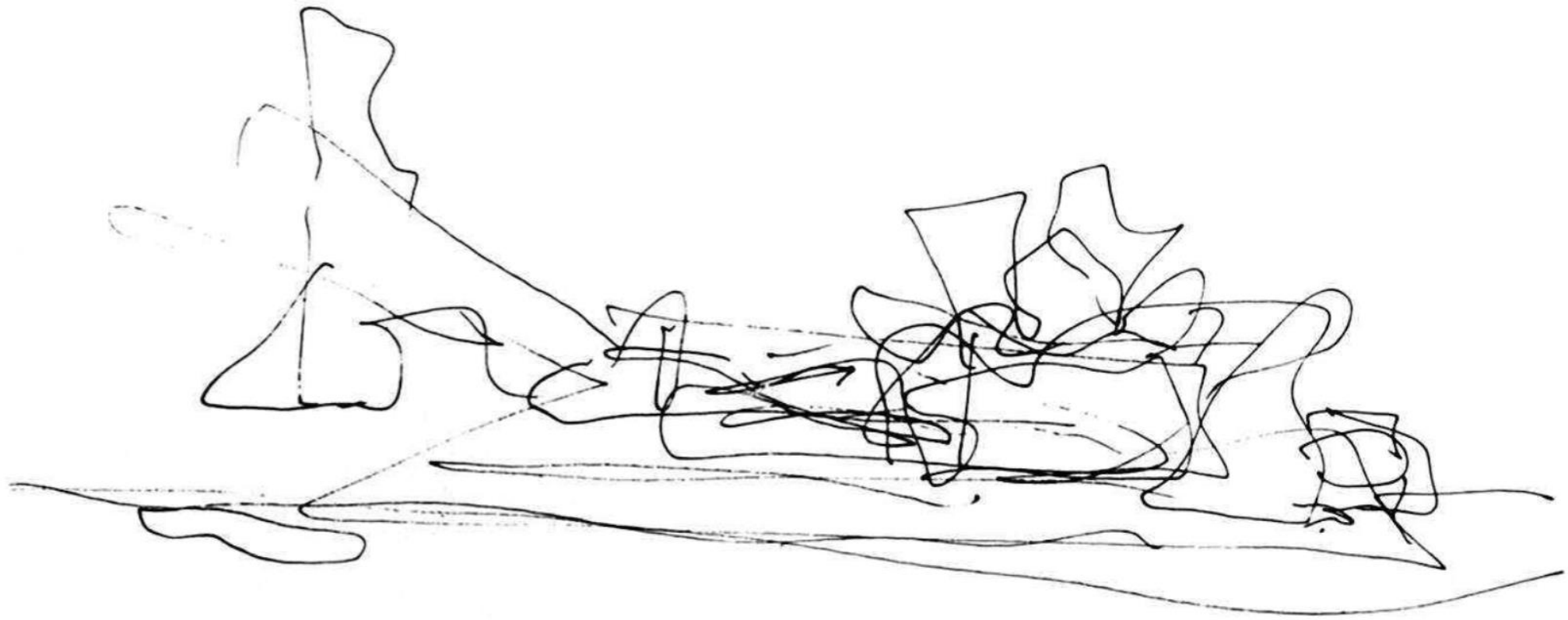


Structural Design & Environmental Impact

Jonas Warmuth

Dr. ès sc. – Postdoctoral researcher, Structural Engineer

context





**iconic structure
won awards**

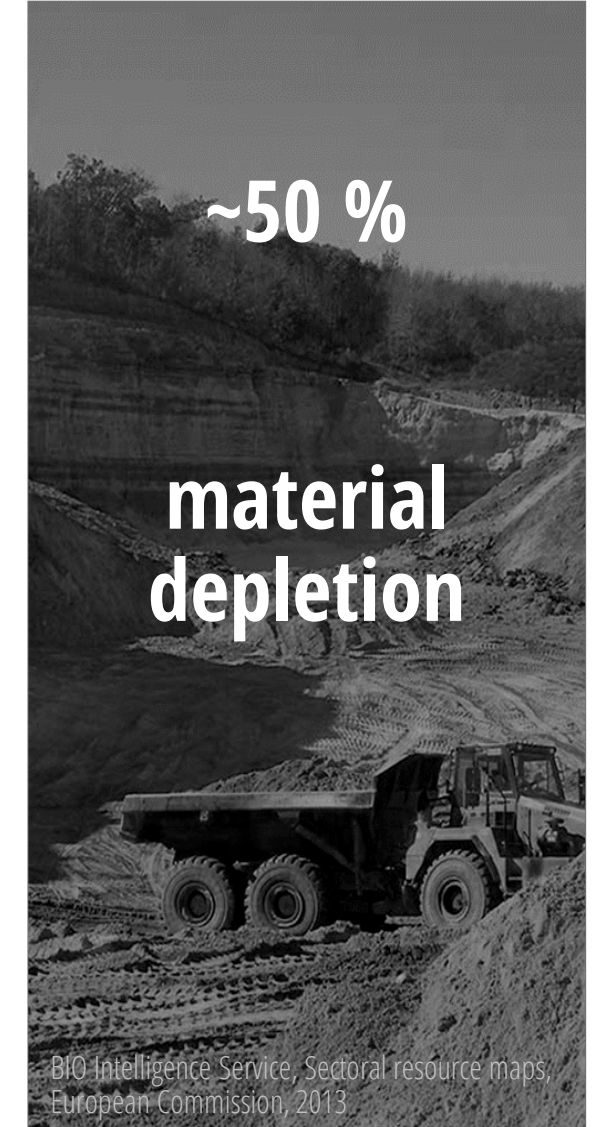
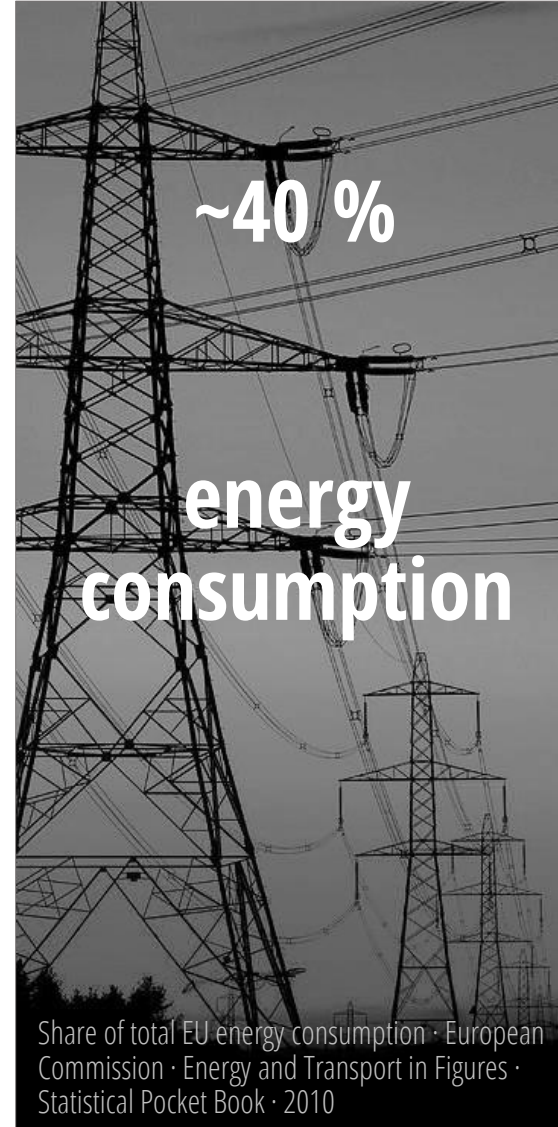
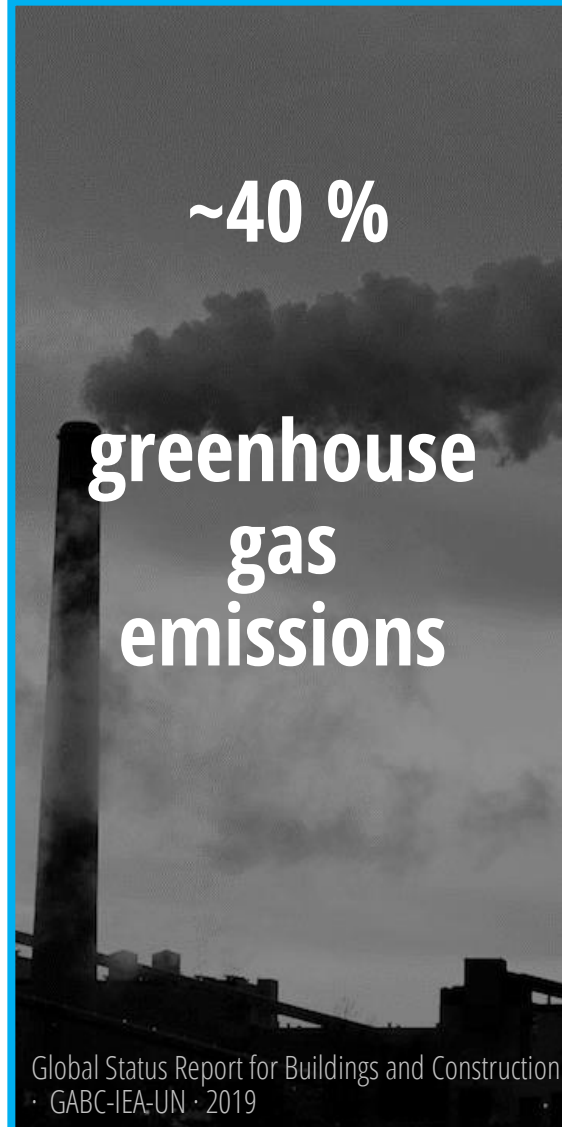
**inefficient loadbearing
material intensive
cost intensive**



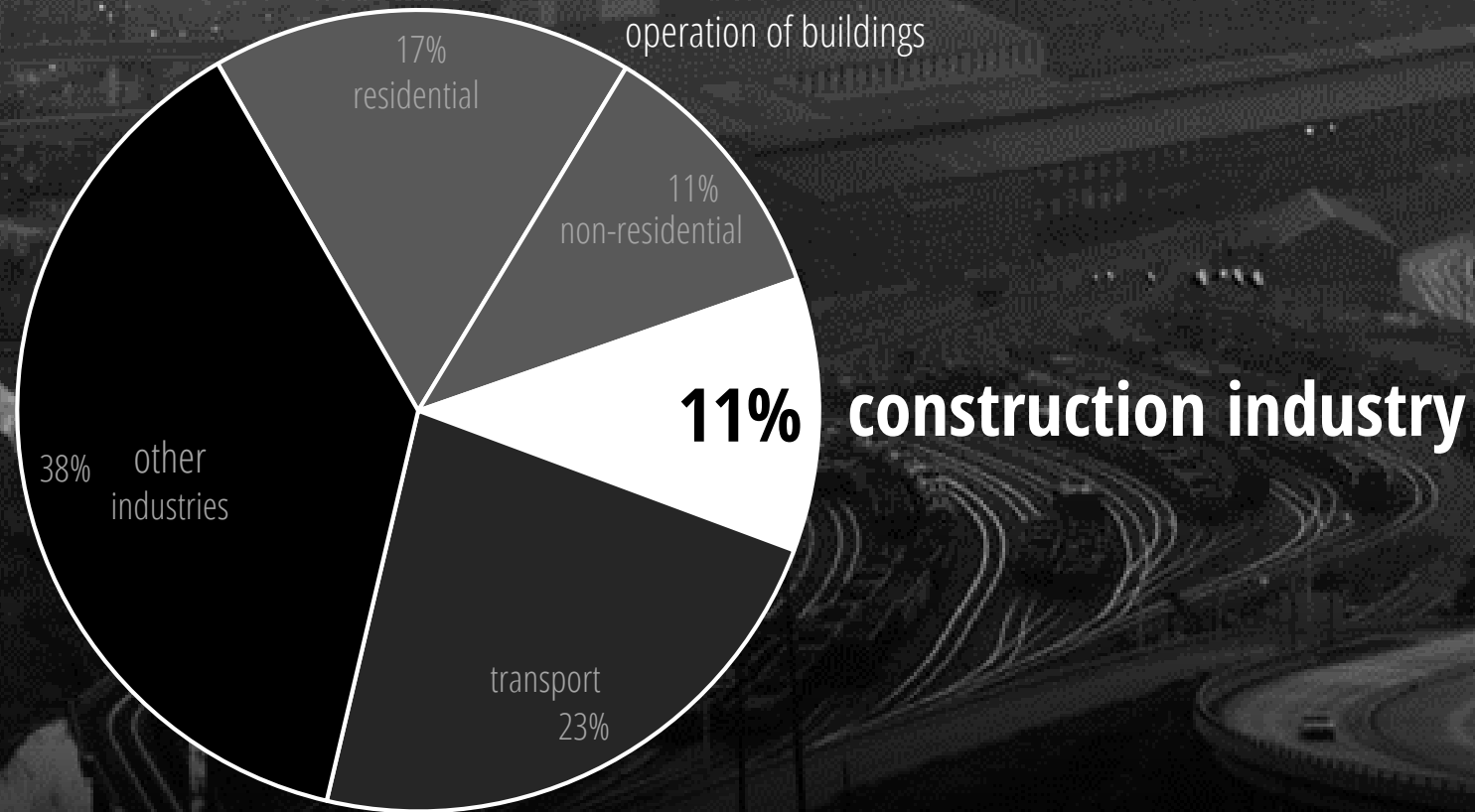
Why might this be an issue?



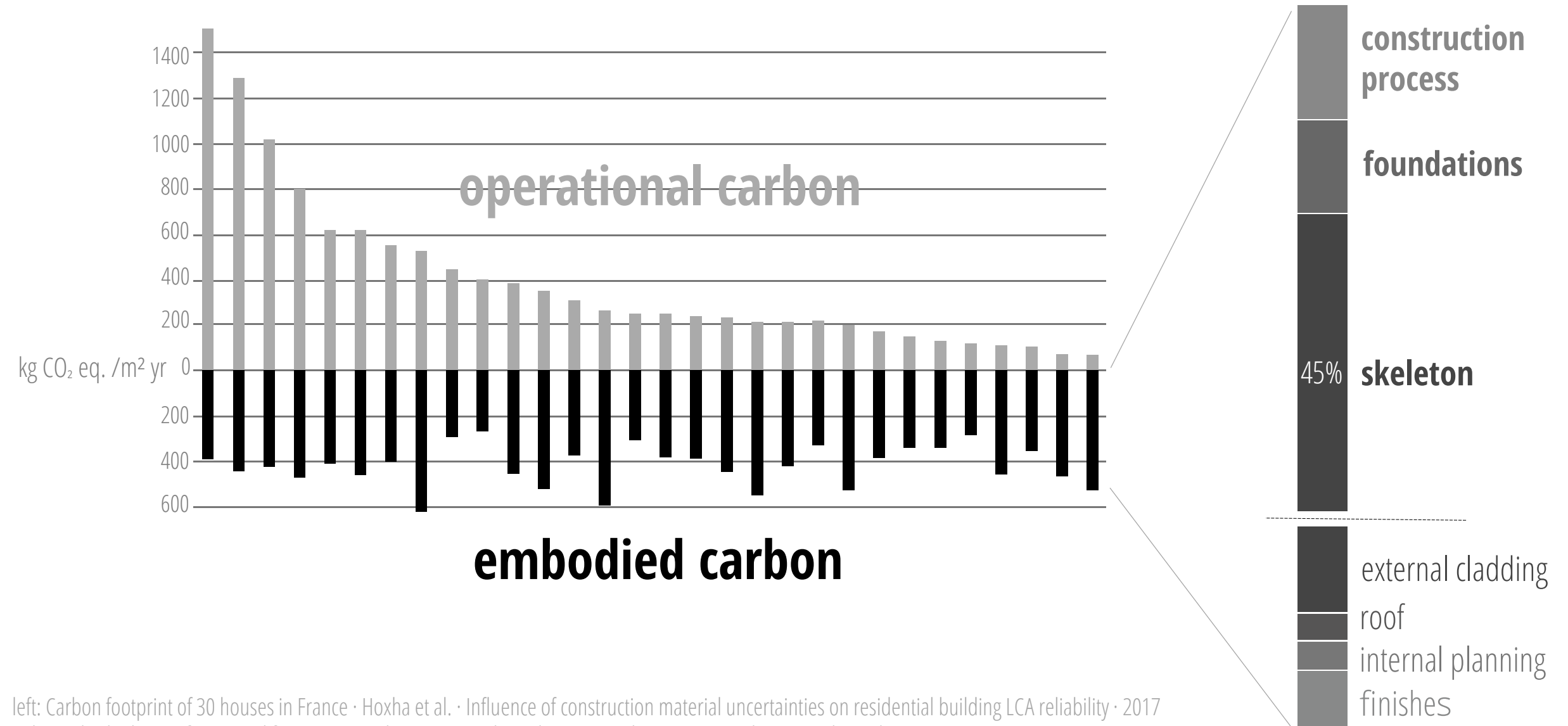
environmental toll of the built environment



anthropogenic global CO₂ emissions



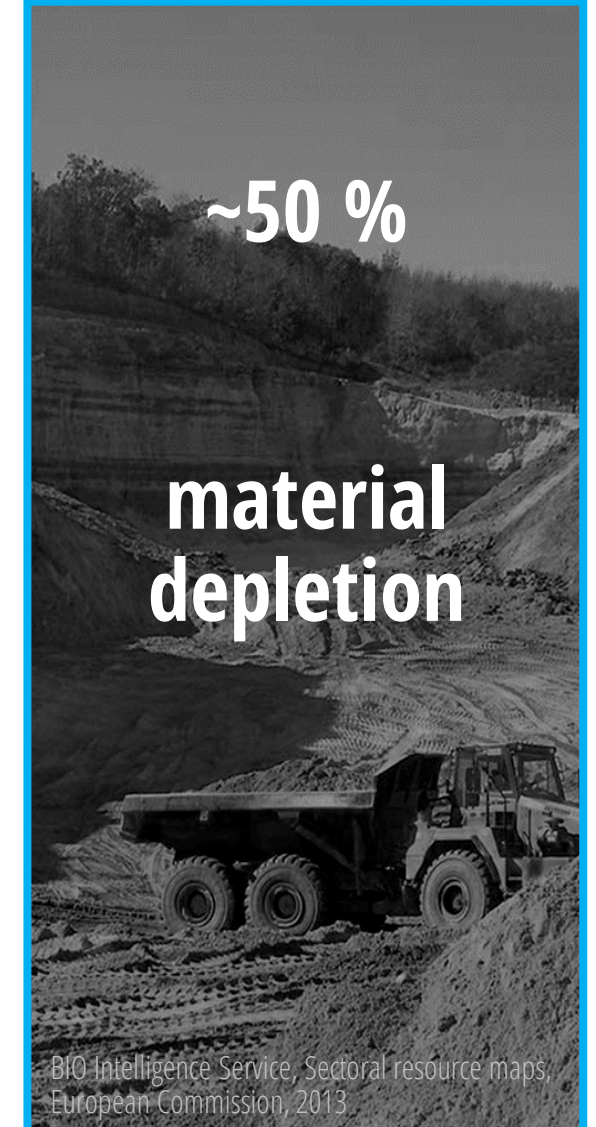
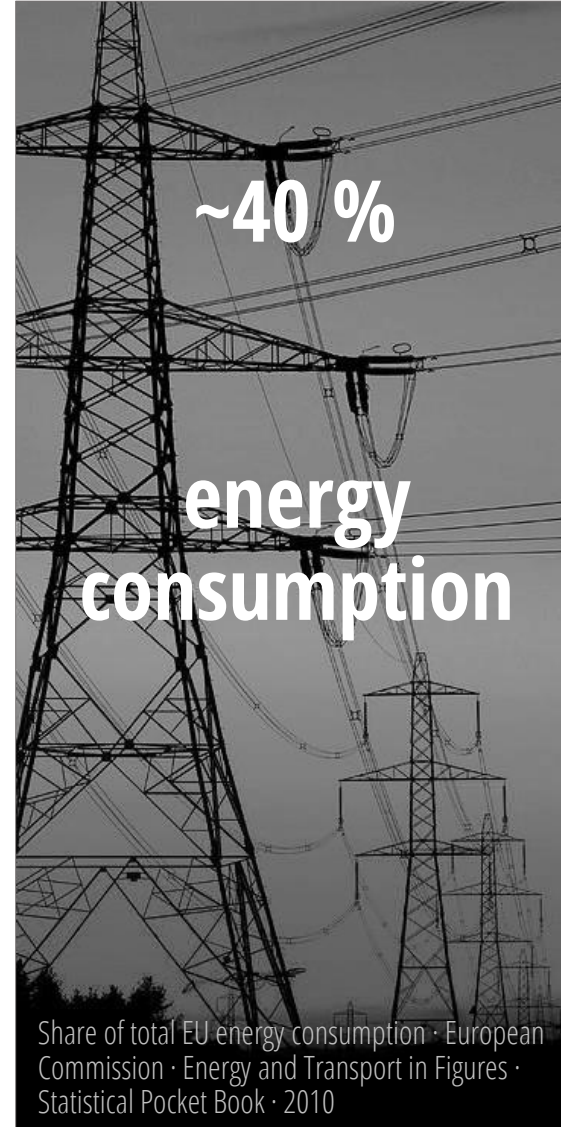
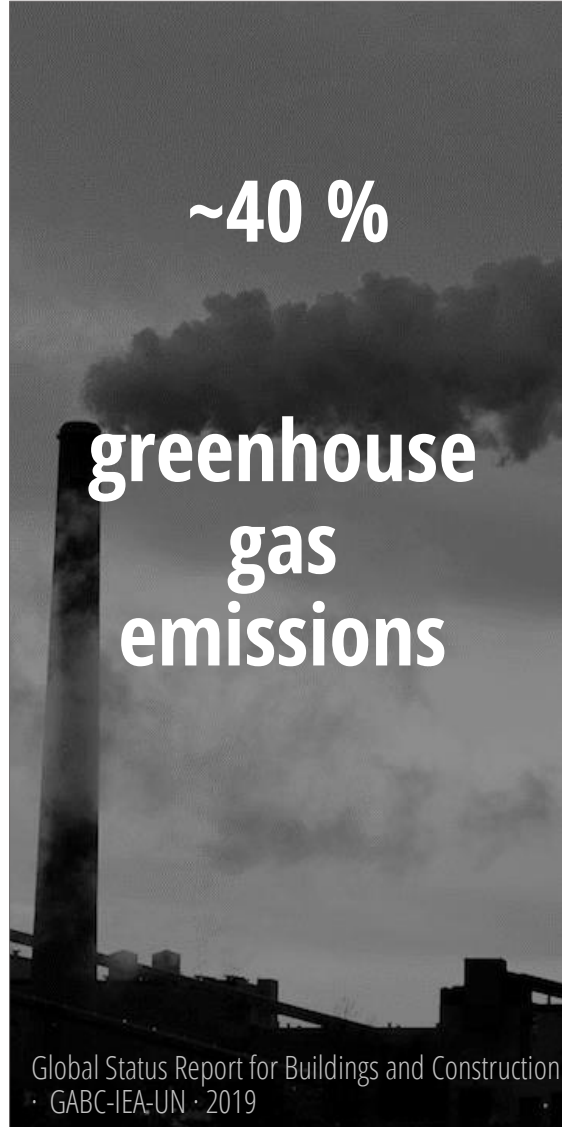
greenhouse gas emissions due to buildings



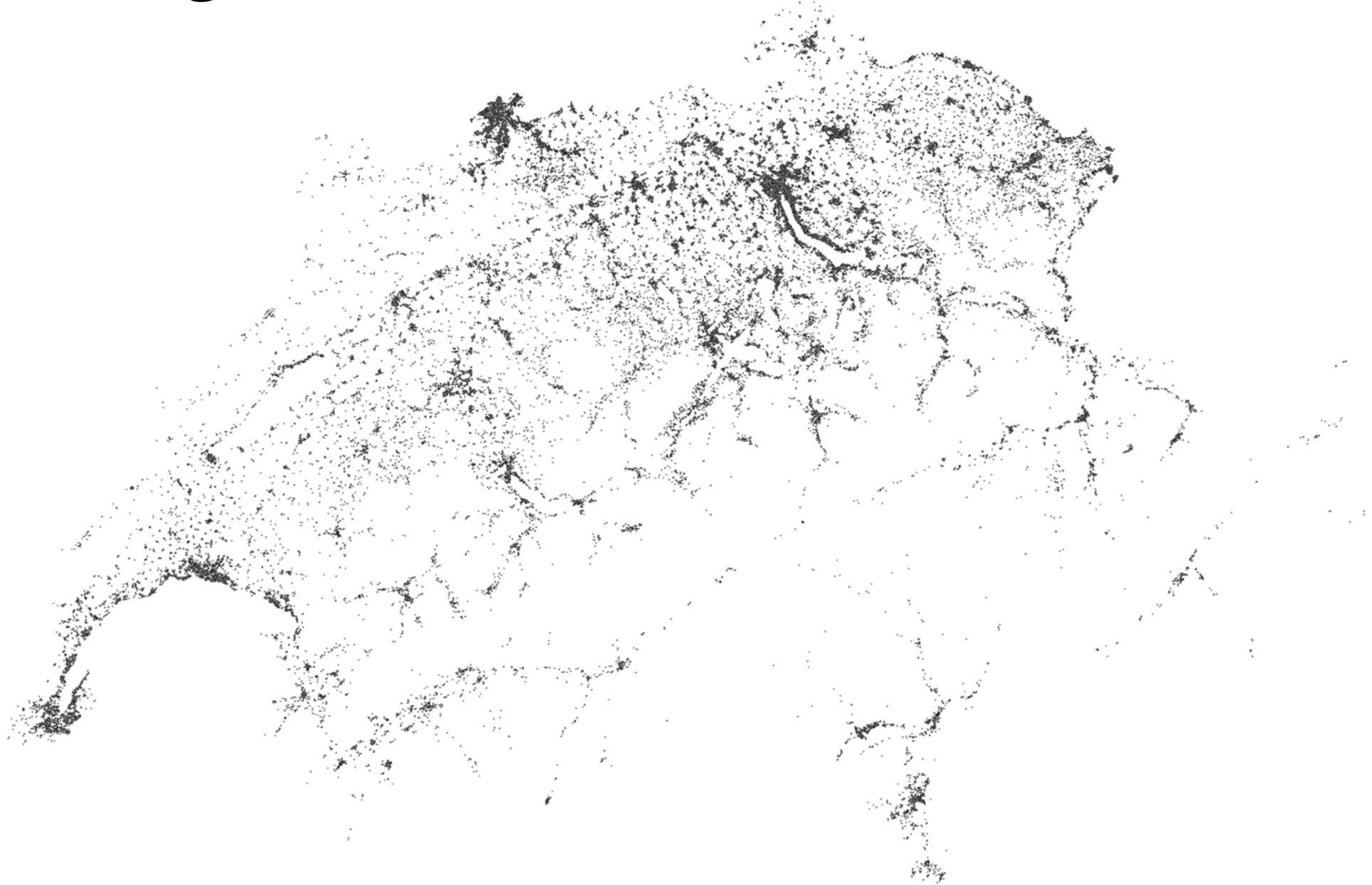
left: Carbon footprint of 30 houses in France · Hoxha et al. · Influence of construction material uncertainties on residential building LCA reliability · 2017

right: Embodied CO₂ of structural frames · S.Kaethner & J.Burridge · The Structural Engineer, London, United Kingdom, pages 33-40 · 2012

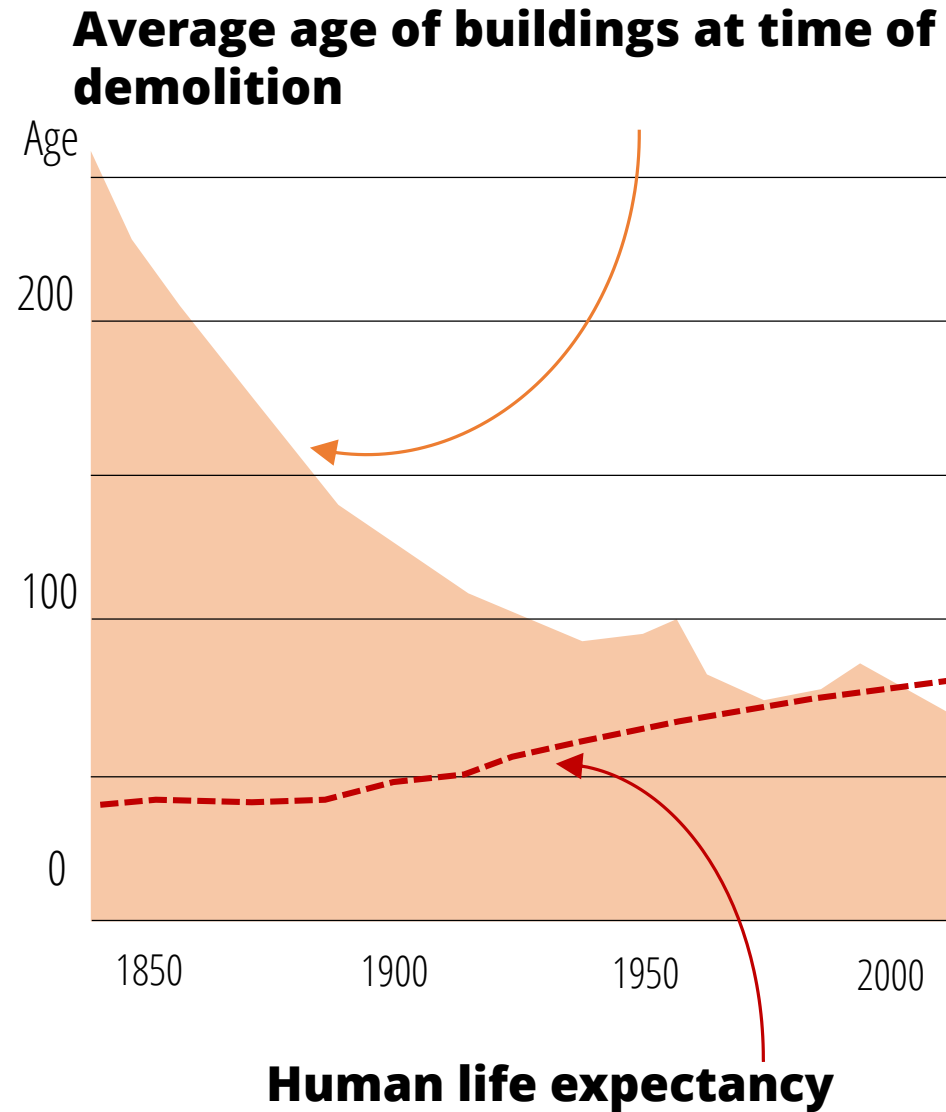
environmental toll of the built environment



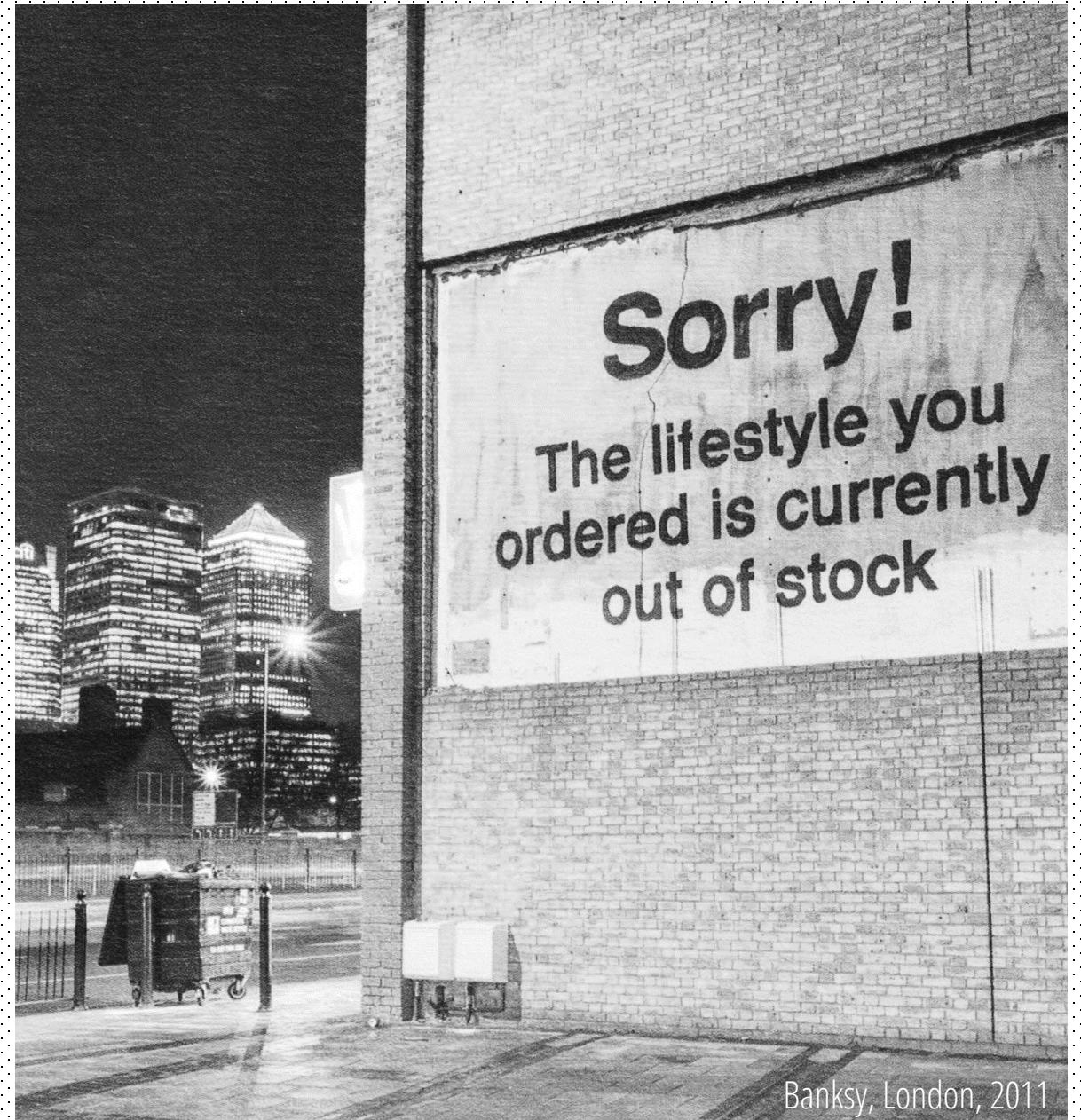
70,000 buildings demolished between 2000 and 2022



changing needs

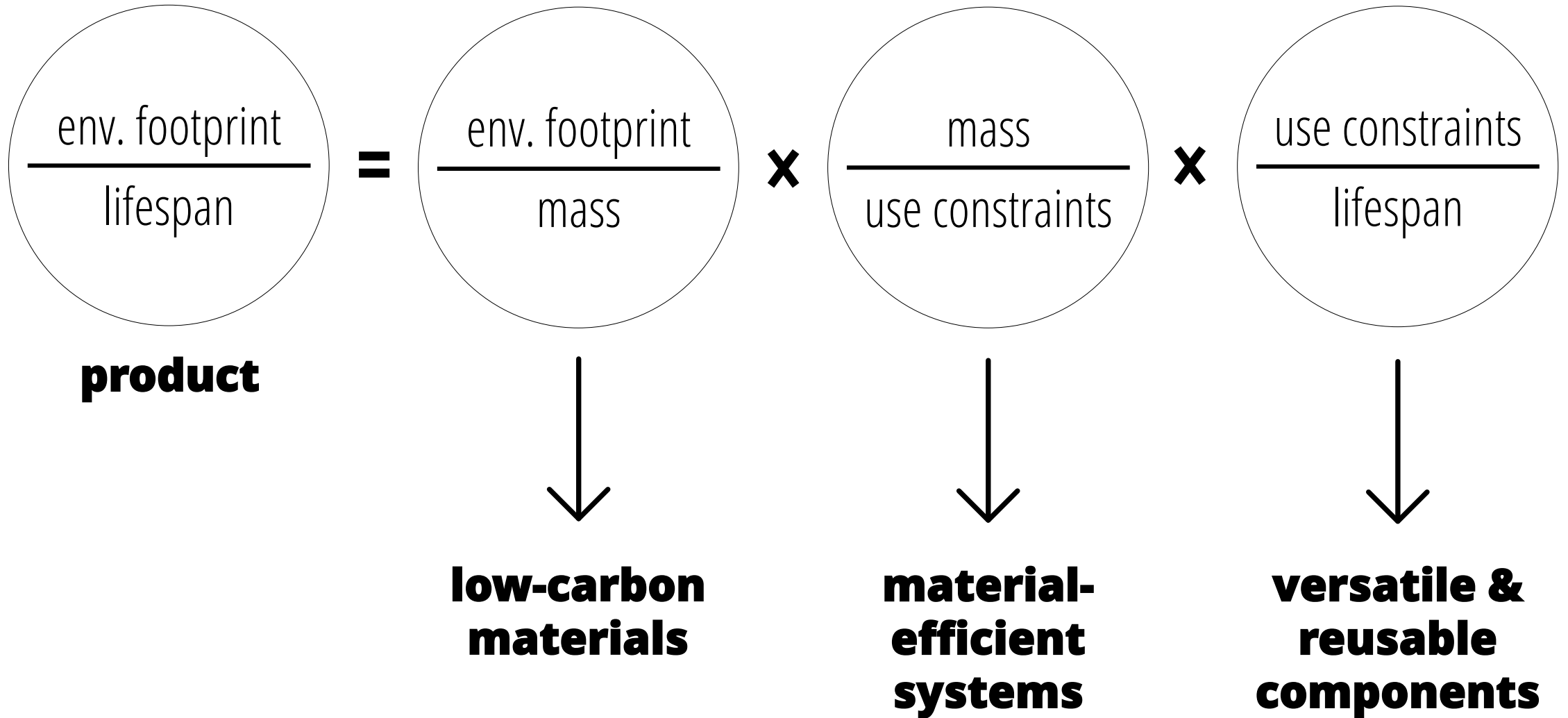


strategies

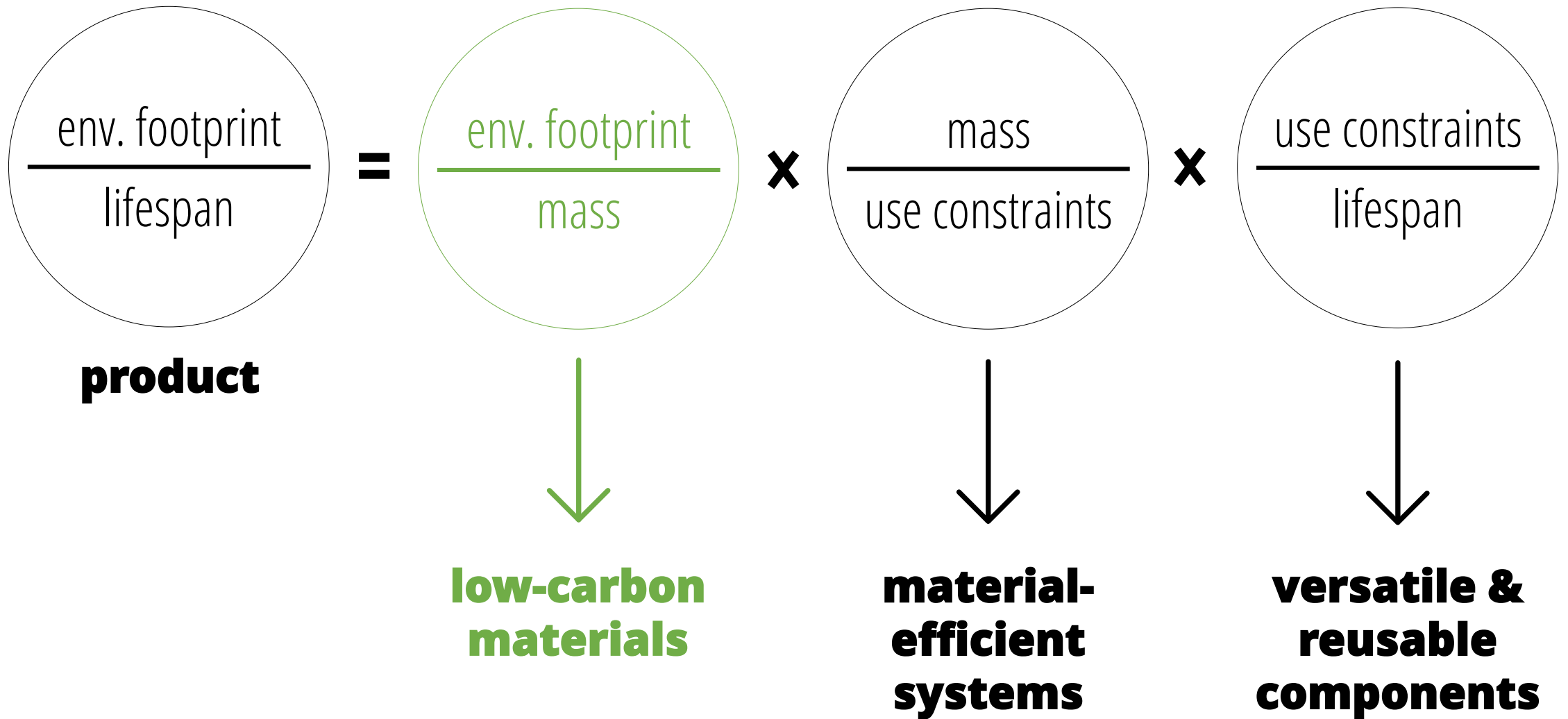


Banksy, London, 2011

a matter of performance and design

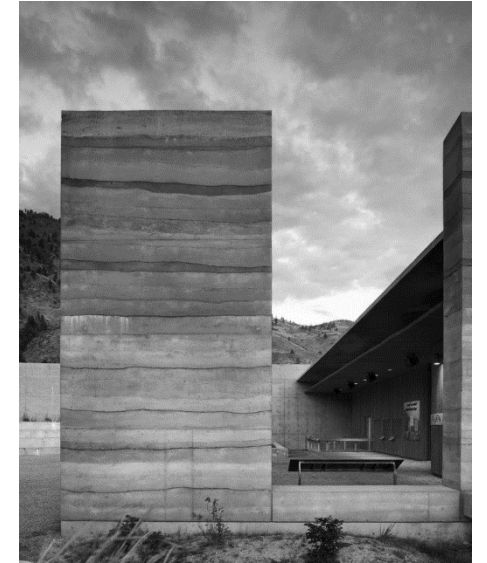


a matter of performance and design



choice of materials

	kgCO ₂ eq/kg
aluminium	8.24
steel	1.77
glass	0.85
plywood	0.81
timber	0.46
bricks	0.22
reinforced concrete	0.15
marble	0.19
stone	0.06



conflicting objectives: example of a bar in tension

steel timber aluminum



conflicting objectives: example of a bar in tension

		<u>steel</u>	<u>timber</u>	<u>aluminum</u>
σ_{allow}	[MPa]	200	7	130
ρ	[kg/m ³]	8000	500	2700
EC	[kgCO ₂ eq/kg]	1.1	0.04	9



conflicting objectives: example of a bar in tension

		<u>steel</u>	<u>timber</u>	<u>aluminum</u>
σ_{allow}	[MPa]	200	7	130
ρ	[kg/m ³]	8000	500	2700
EC	[kgCO ₂ eq/kg]	1.1	0.04	9



carbon footprint [kgCO₂eq]

= **carbon coeff.** [kgCO₂eq/kg] **x mass** [kg]

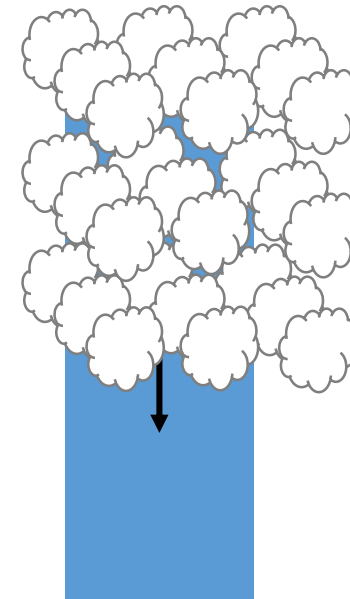
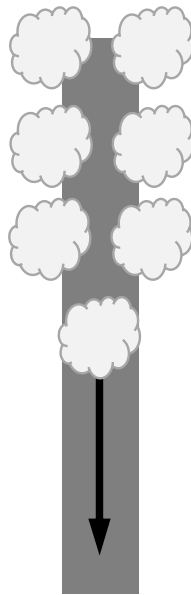
= ρ [kg/m³] **x volume** [m³]

= **length** [m] **x cross section** [m²]

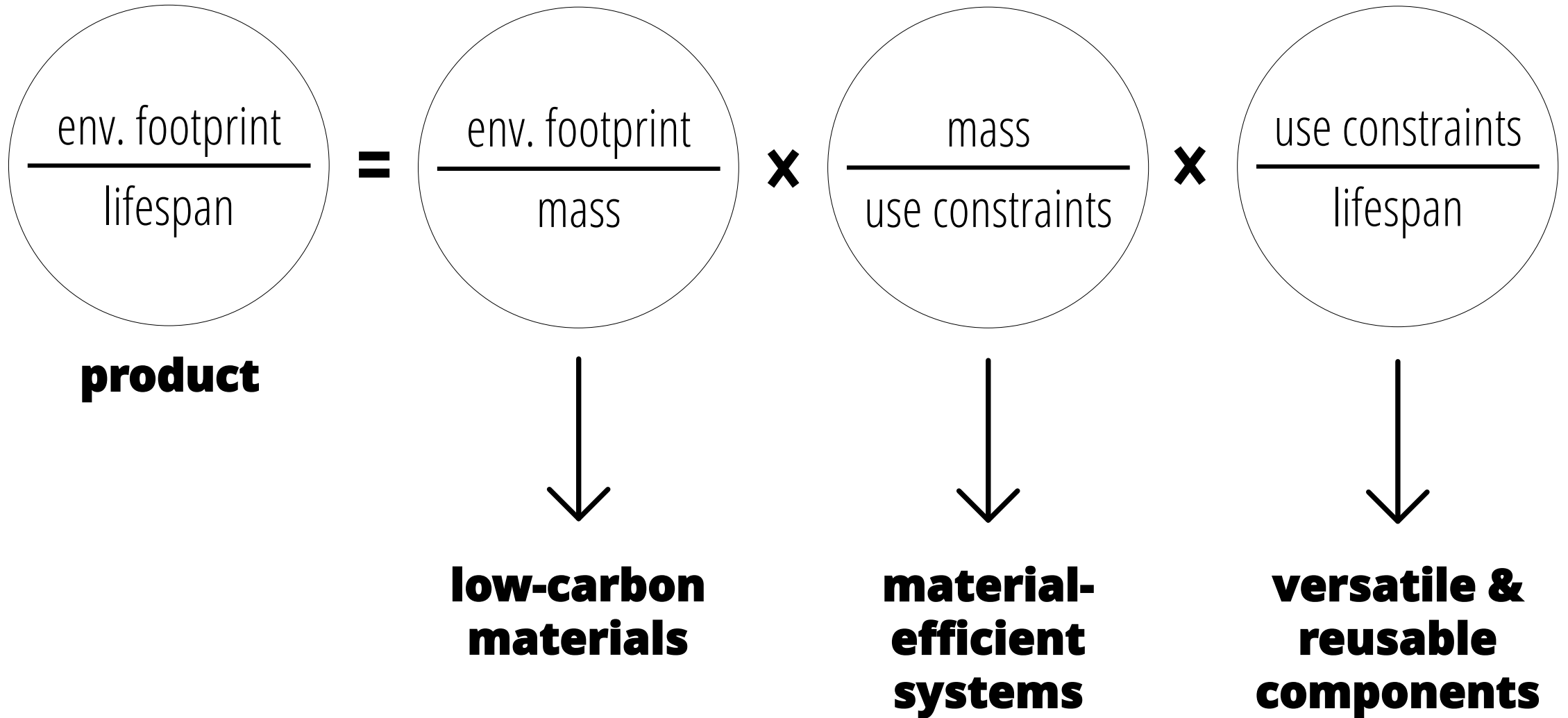
= **force** [kN] **x** σ_{allow} [kN/m²]

conflicting objectives: example of a bar in tension

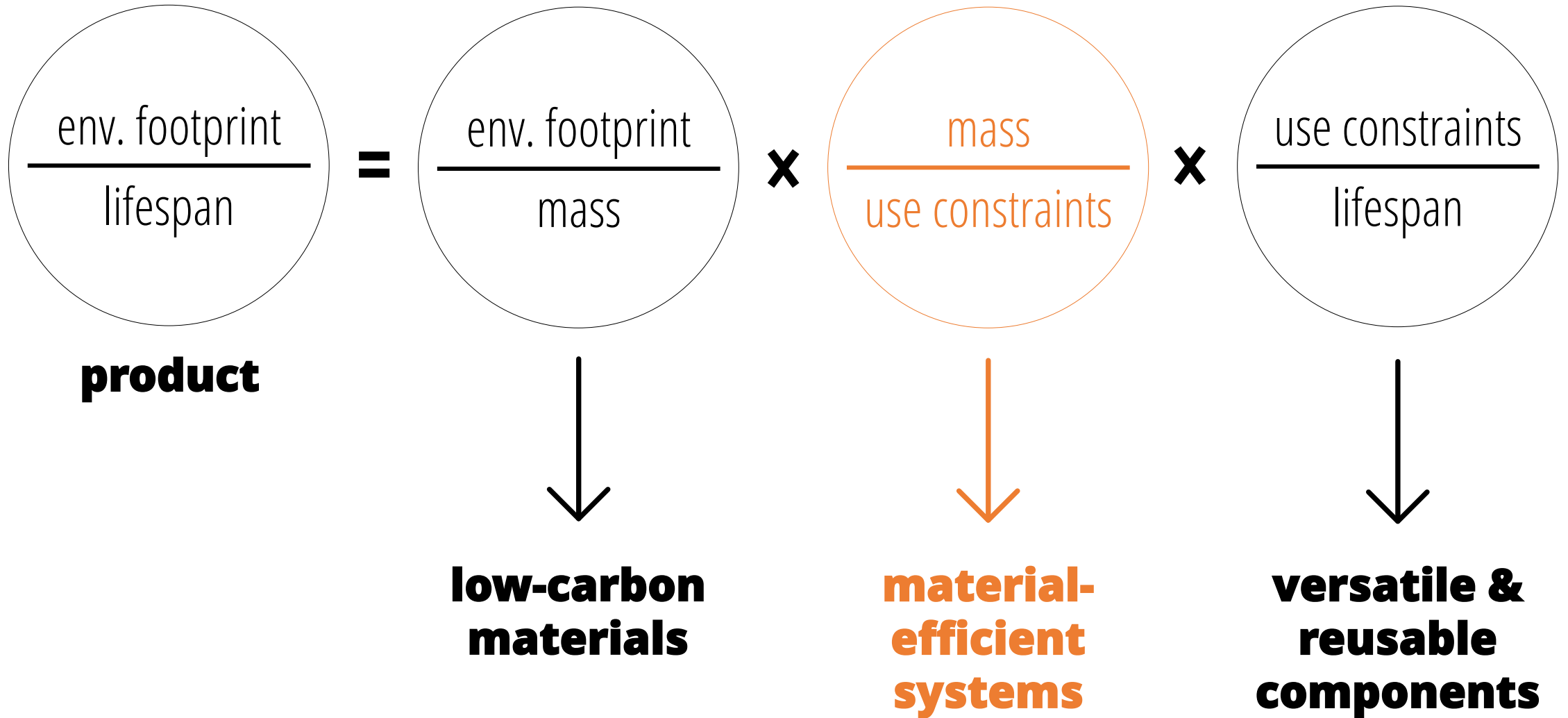
	<u>steel</u>	<u>timber</u>	<u>aluminum</u>
volume [cm ³]	500	14285	770
mass [kg/m ³]	4	7	2
EC [kgCO ₂ eq/kg]	4.4	0.3	18



a matter of performance and design



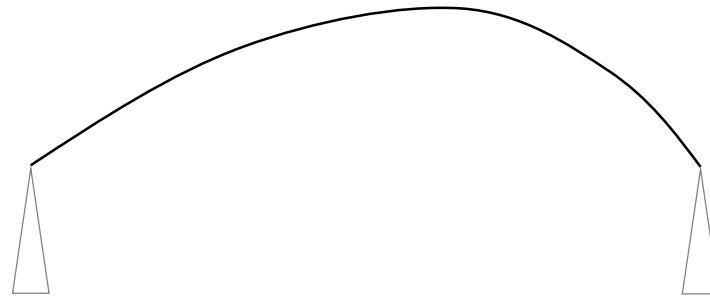
a matter of performance and design



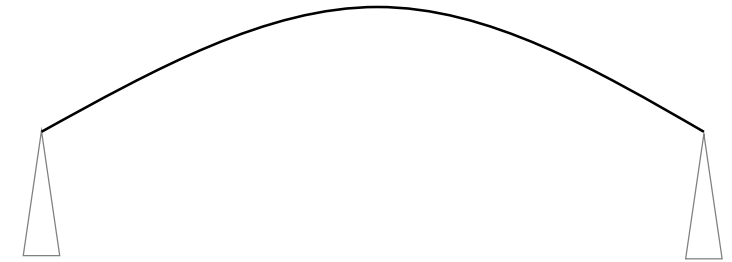
why form matters



$$V = 0.75$$



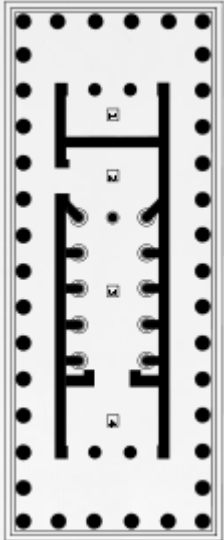
$$V = 0.50$$



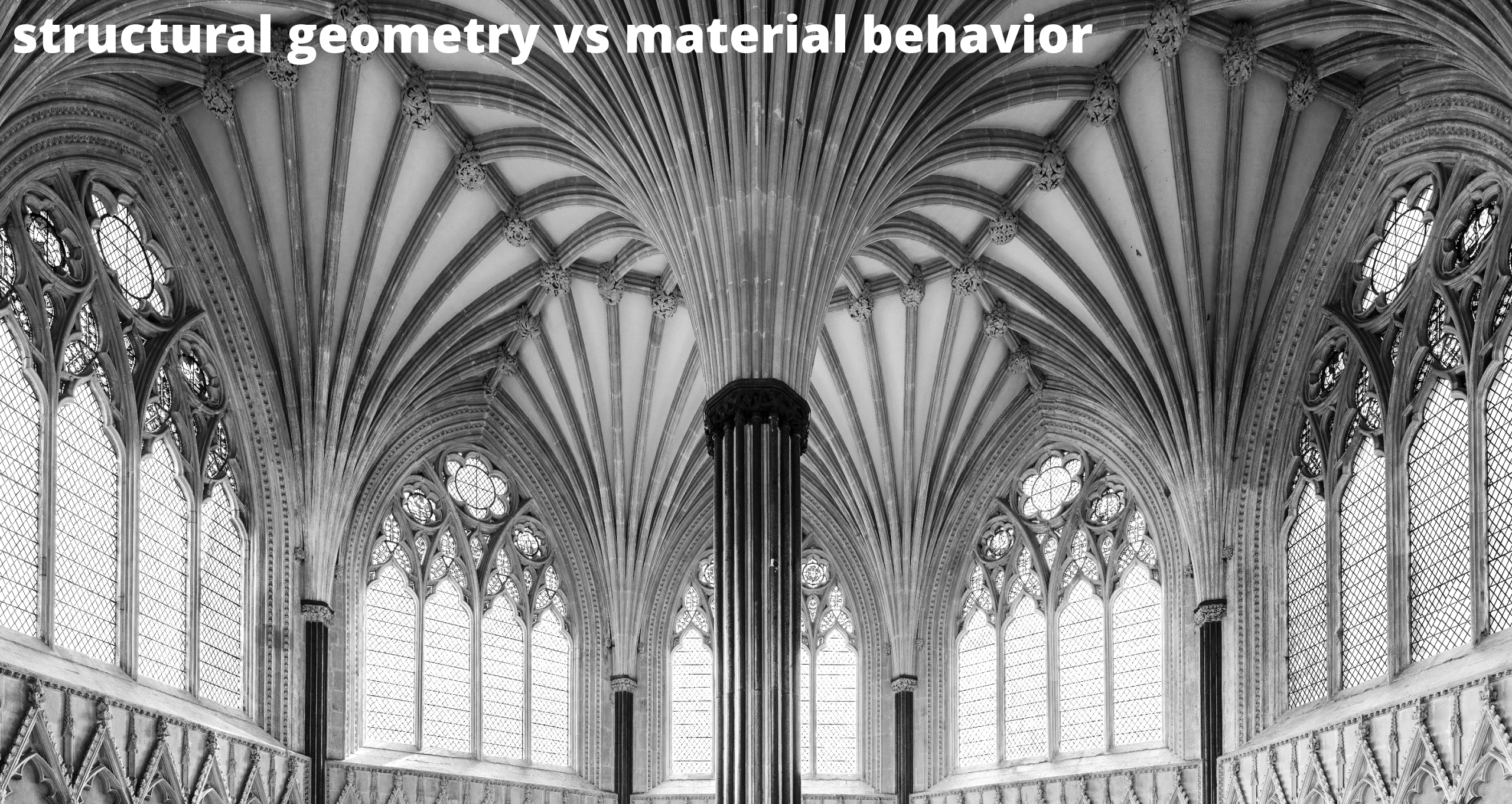
$$V = 0.25$$

› form matters!

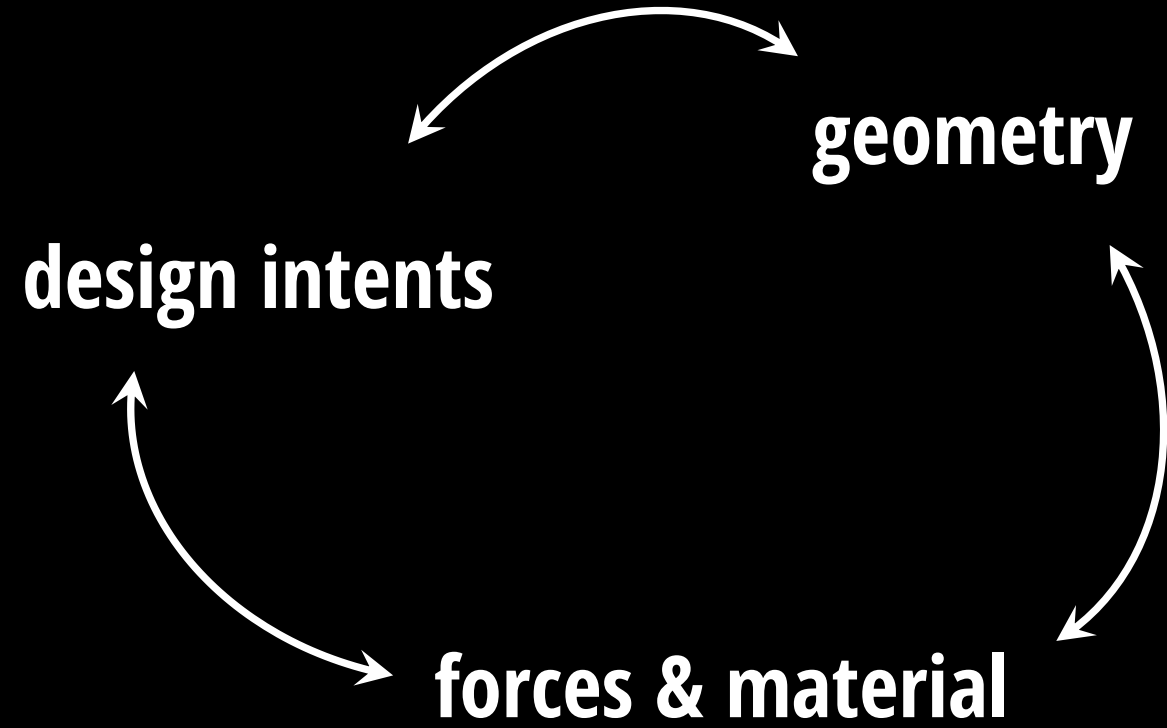
structural geometry vs material behavior



structural geometry vs material behavior



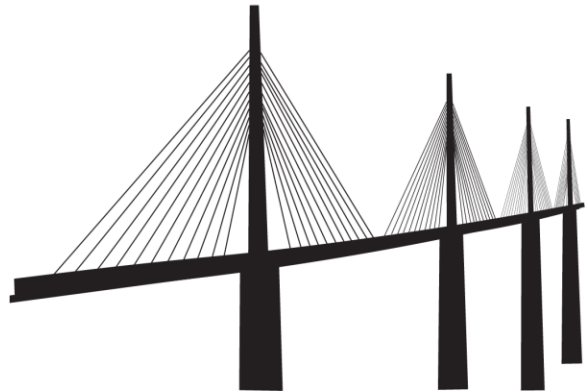
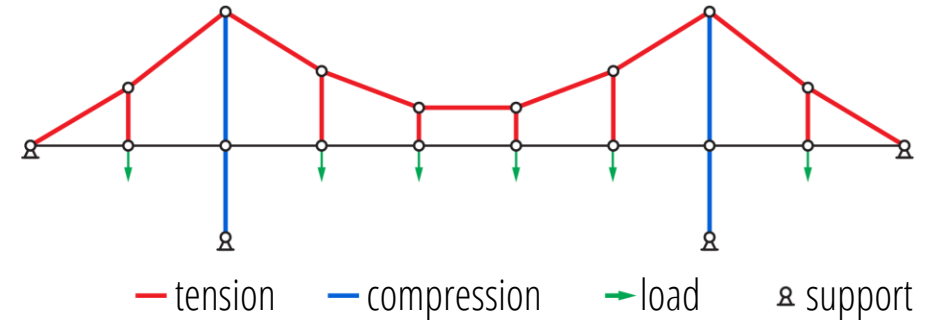
structural design



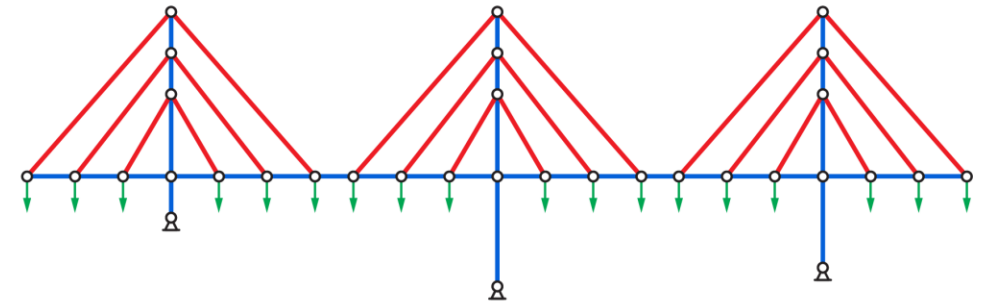
discrete equilibrium models



translation →



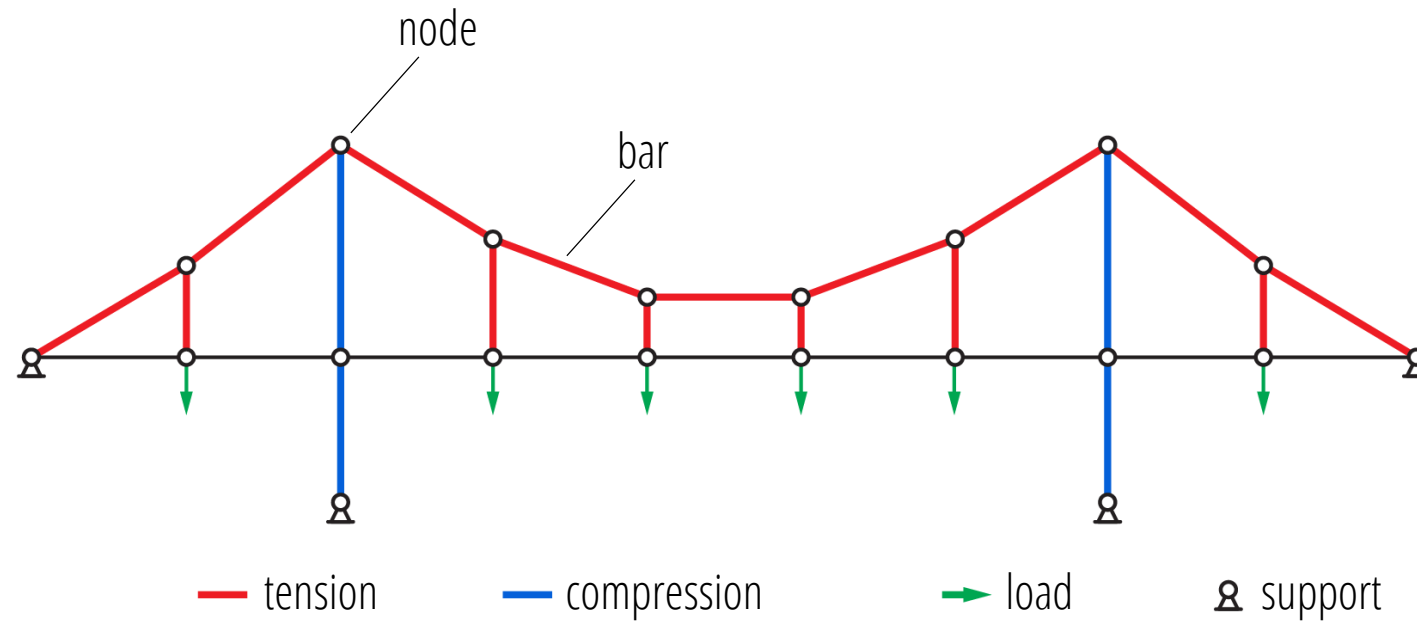
translation →



real structure

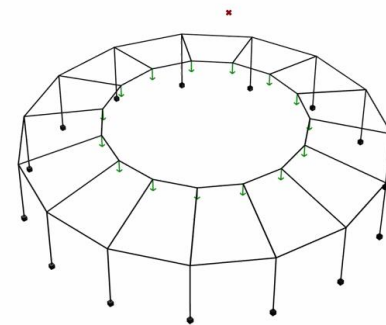
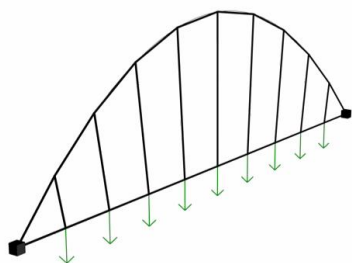
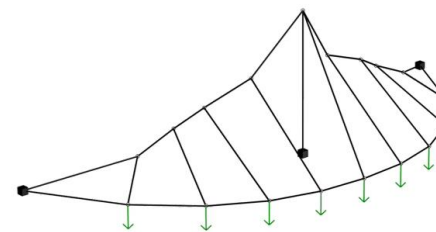
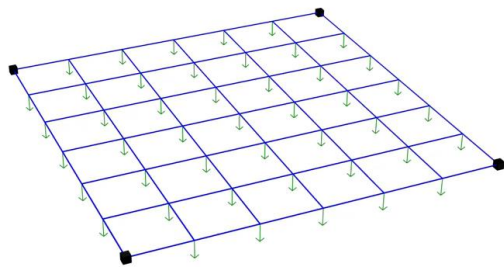
discrete equilibrium model

discrete equilibrium models (DEMs)

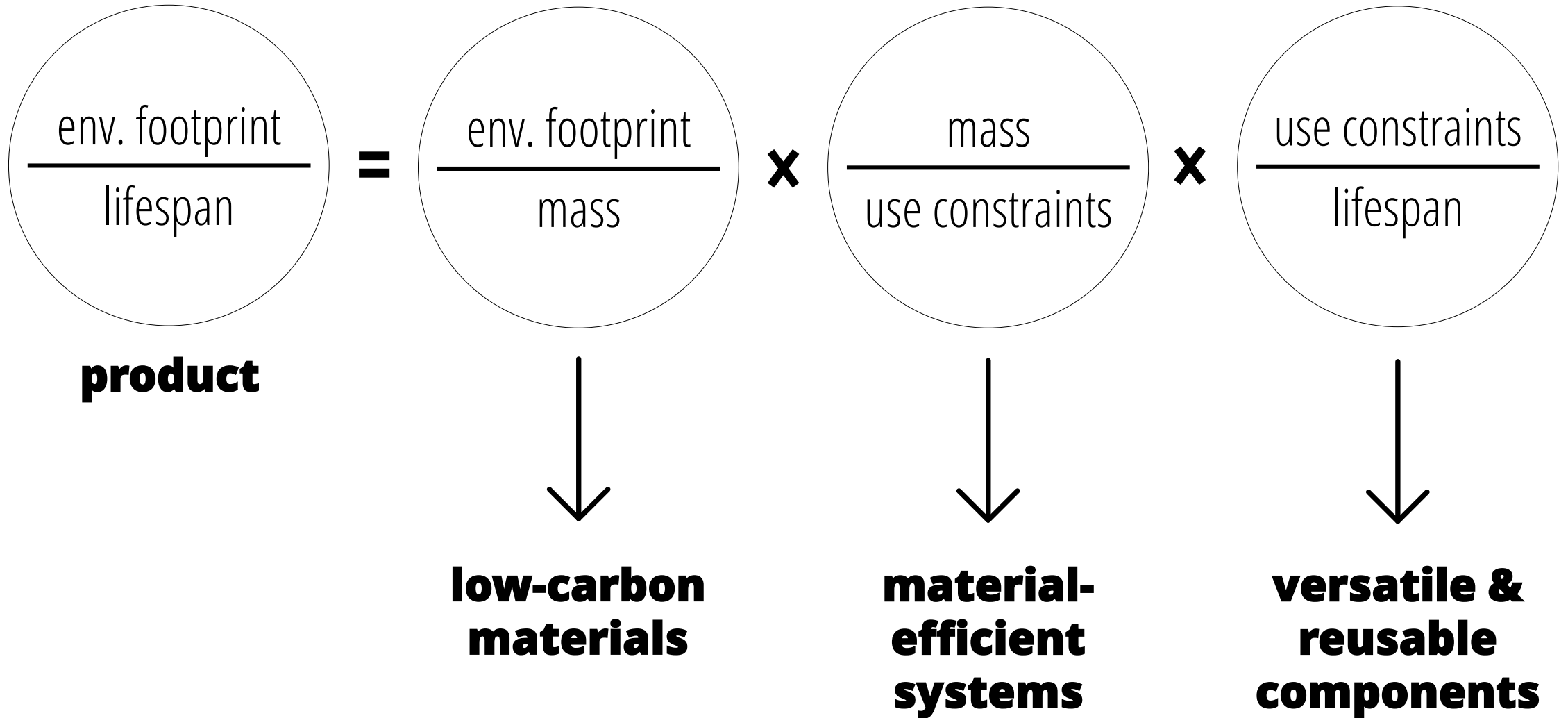


topology connectivity of the graph

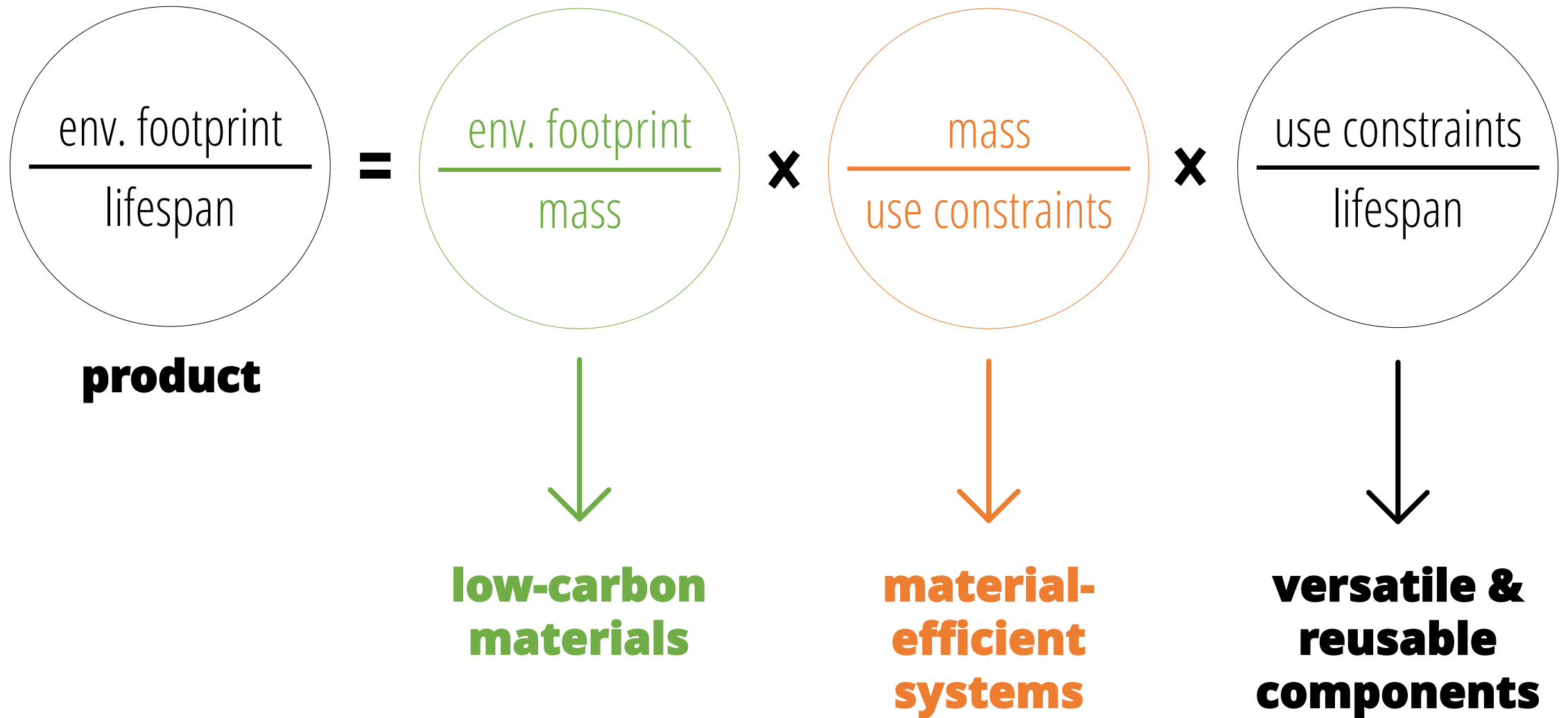
geometry position of the nodes

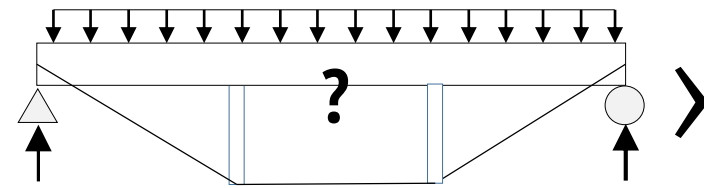


a matter of performance and design



a matter of performance and design





> **applied loads**
 $q = \dots \text{ kN/m}$ (dead load, snow, wind,...)

> **static equilibrium**
 $\sum H=0$
 $\sum V=0$
 $\sum M=0$

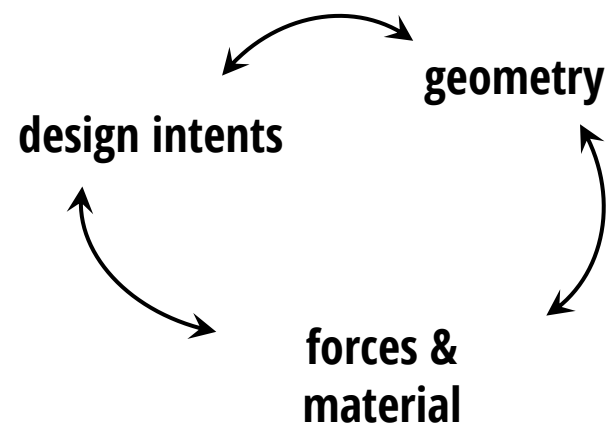
> **compatibility** (deformations & displacements)

> **stress limits**
 $\sigma \leq \dots$

> **serviceability limits**
 $\delta \leq \dots$

> **cross sections**
 $A = \dots$
 $EI = \dots$

> **construction**

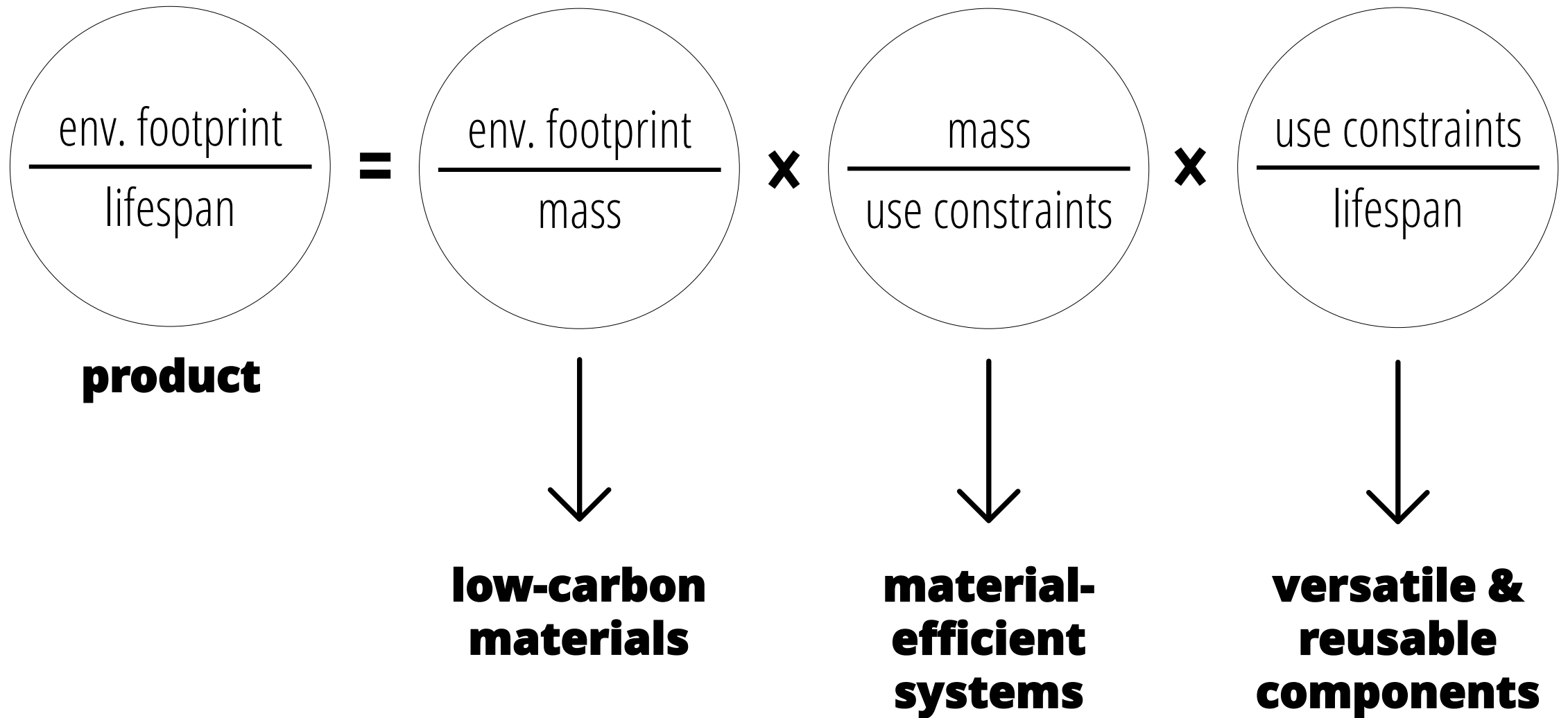


> **environmental impact**

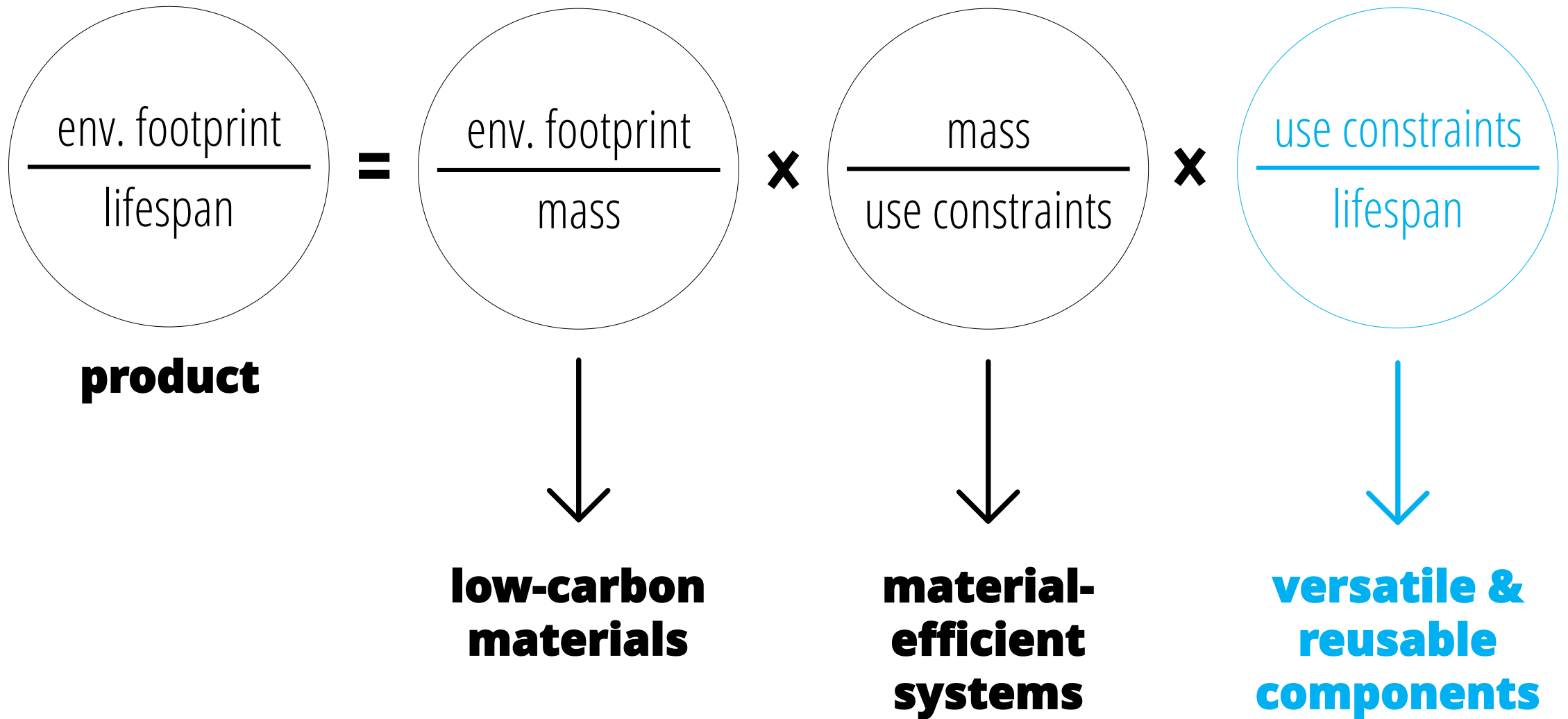
$$EI = \sum_{i=0}^{\text{material}} EC_i \times MASS_i$$

$\text{kgCO}_2\text{eq/kg}$ kg/unit

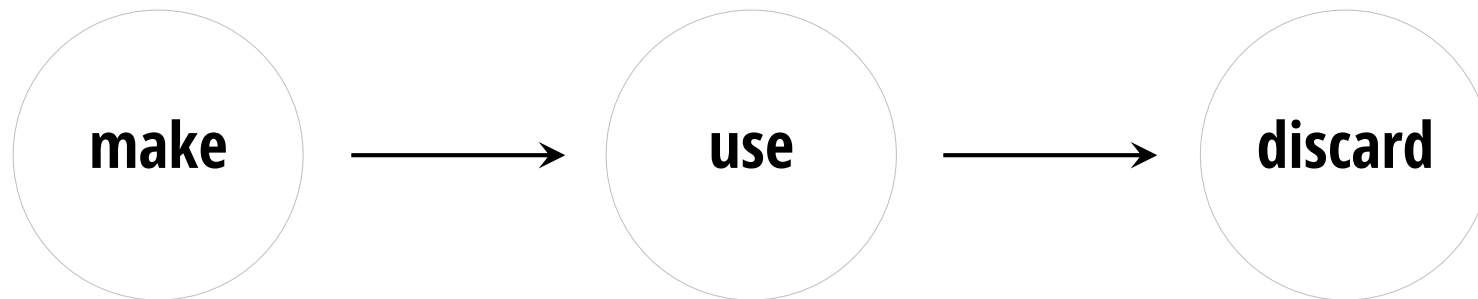
a matter of performance and design



a matter of performance and design

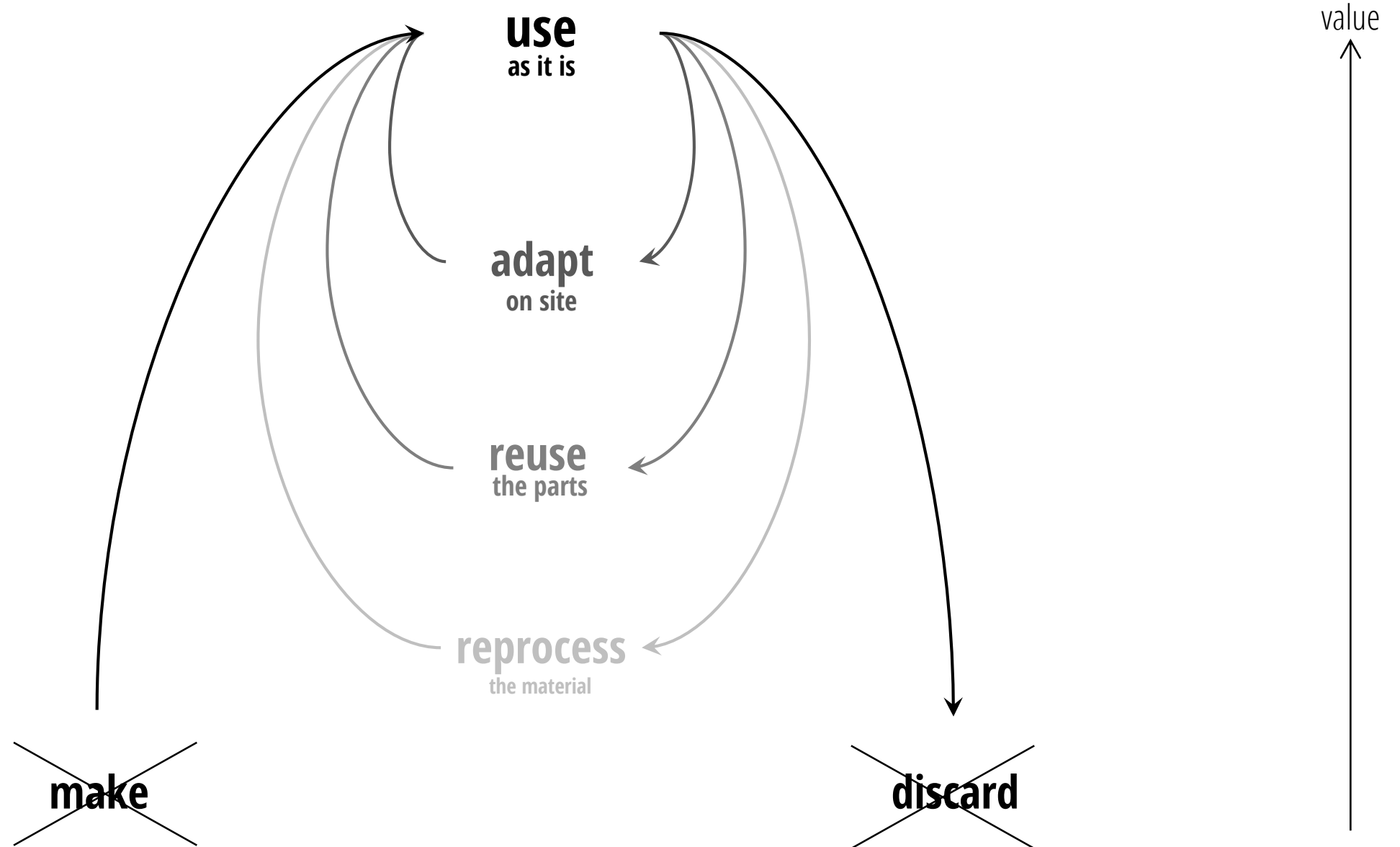


from linear to...



circular economy

= maximize service life of existing products



Timber bridge - Eglisau, CH



constructed in 1810



deconstructed in 1919

Timber barn – Kloster Rheinau, CH



reused in 1920



state 2022

reuse was common in the past...



...and it is today(?)



...and it is today(?)



...and it is today(?)





Olympic Stadium, London (UK), 2012

Architects: Populous
Engineers: Buro Happold



Reuse of second-hand gas pipeline tubes in the stadium roof truss.



K118, Winterthur

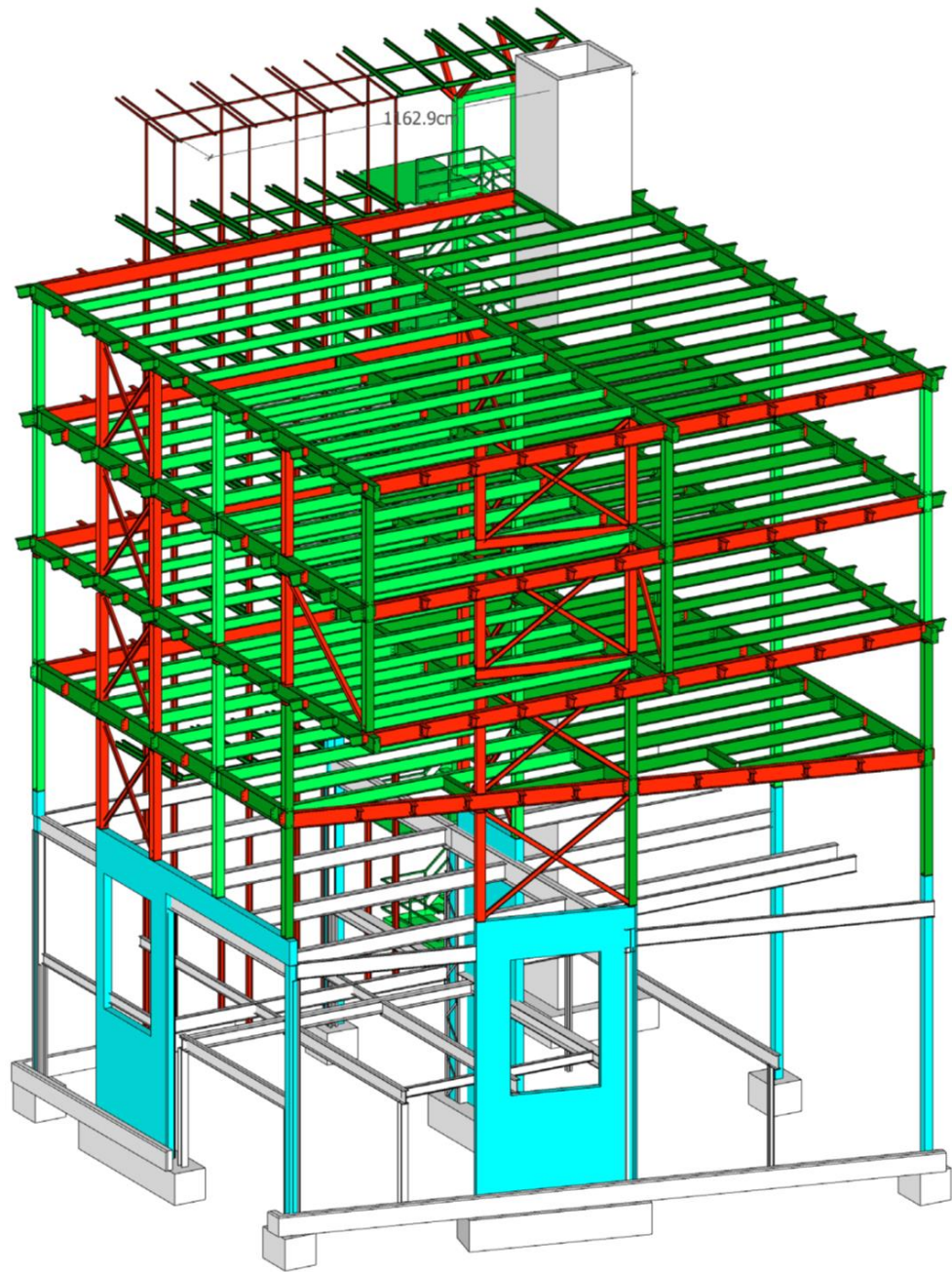
Architects: in.situ



Reuse of steel structure elements from warehouses.



K118, Winterthur
Architects: in situ



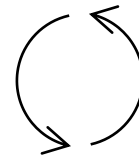
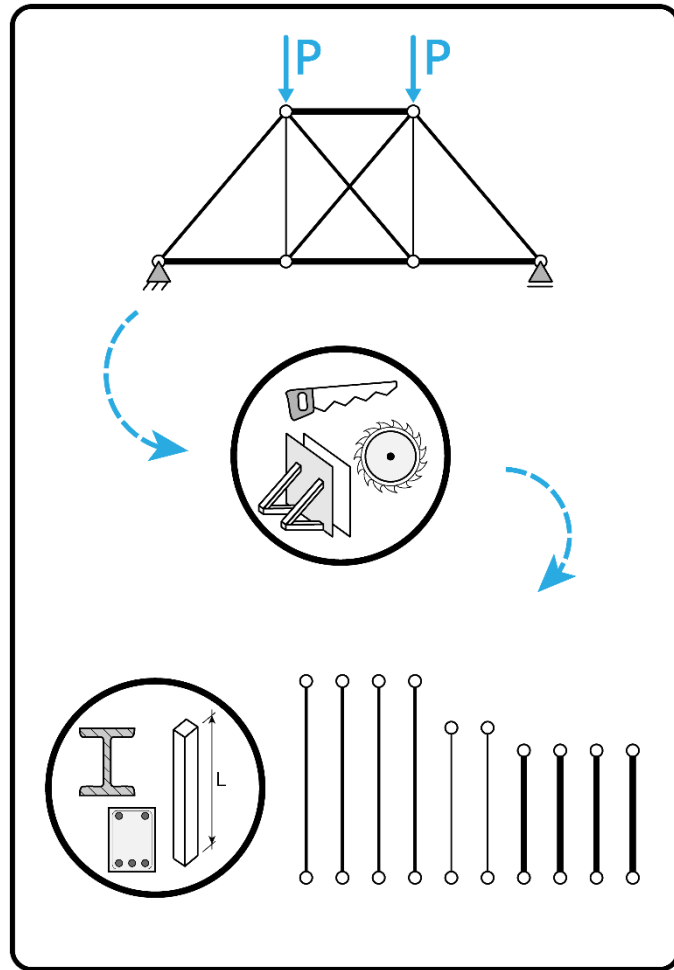
K118, Winterthur

Architects: in situ

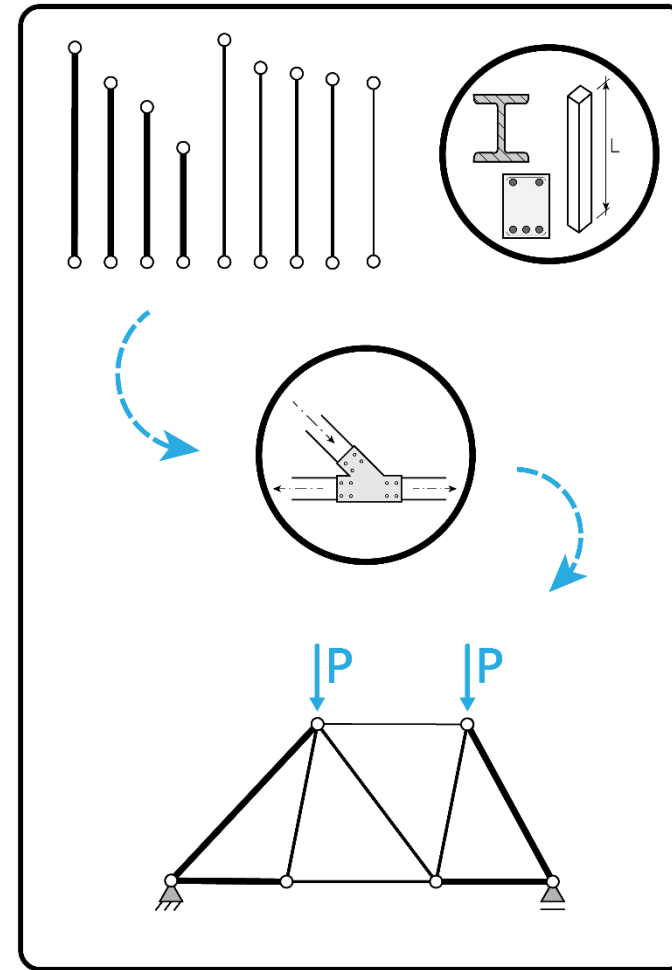
Reuse of steel structure elements from warehouses.

change of design paradigm

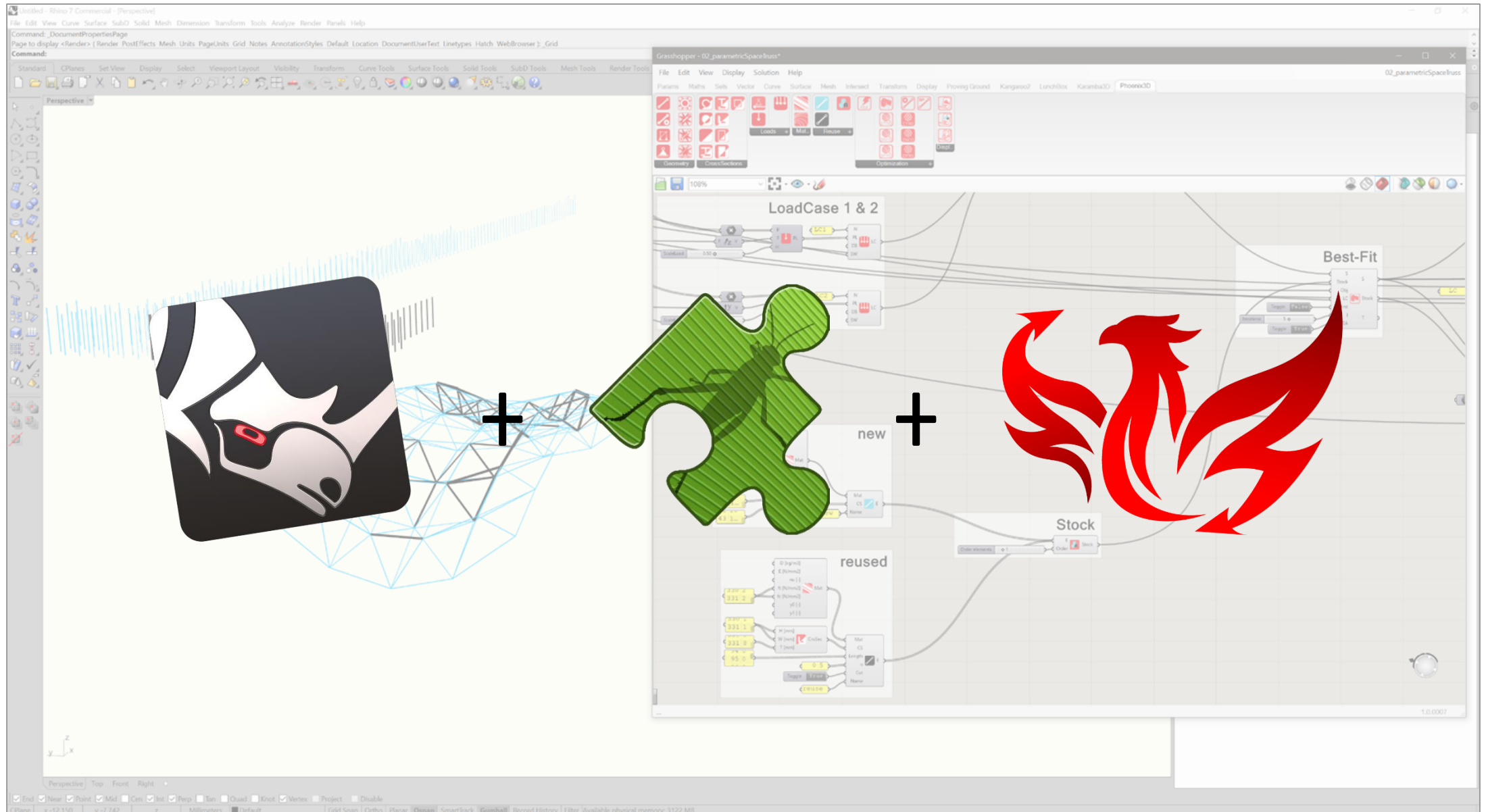
conventional design



design through reuse



phoenix3d



File Edit View Curve Surface SubD Solid Mesh Dimension Transform Tools Analyze Render Panels Help
 Grasshopper file (Browse): "C:\Users\jonas\Box\PROD B12 - upcycling design of structures (JW)\03_seminars\2023_workshop_TUD\Rhino\pavillon_design_idea.gh"
 Grasshopper option (Window Document Solver Banner): _Enter
 Grasshopper option (Window Document Solver Banner)
 Command: |

Standard CPlanes Set View Display Select Viewport Layout Visibility Transform Curve Tools Surface Tools Solid Tools SubD Tools Mesh Tools Render Tools Drafting New in V7

Perspective

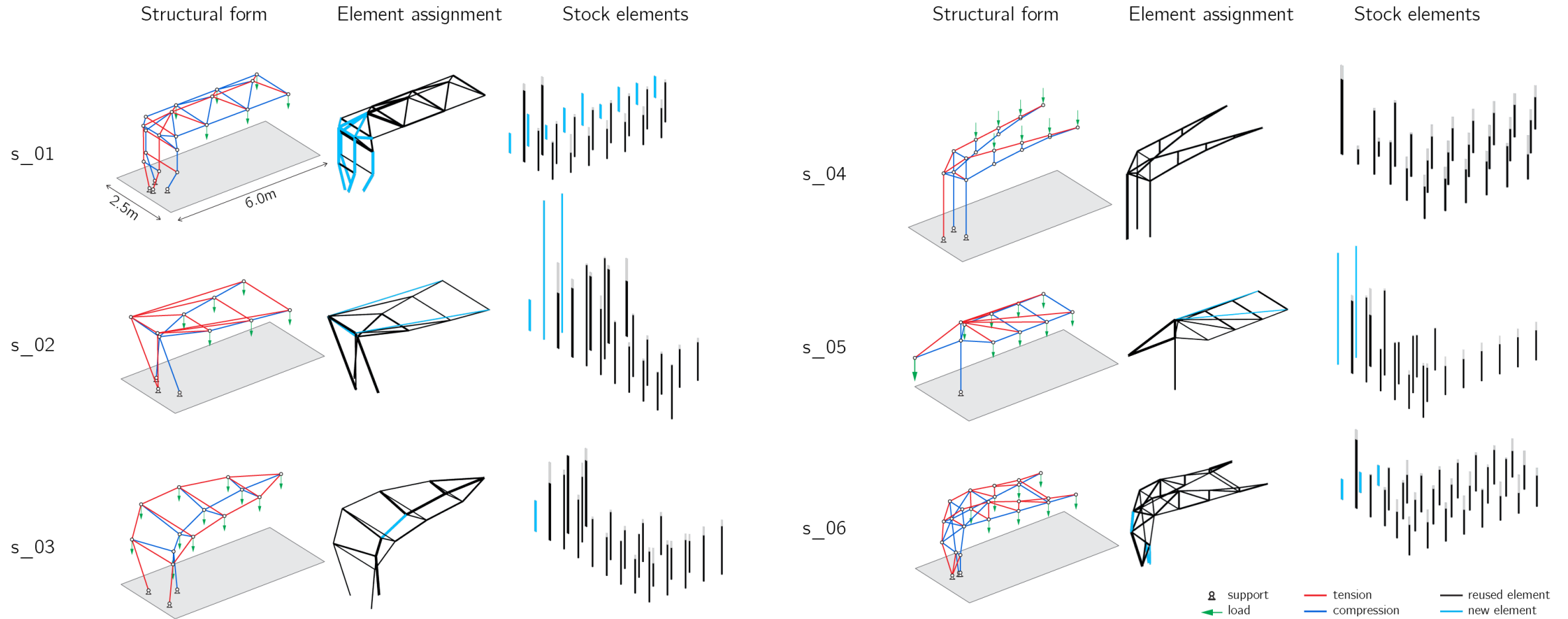
Layers
 Layer Default

End Near Point Mid Cen Int Perp Tan Quad Knot Vertex Project Disable
 CPlane x 73.222 y 3.526 z 0 -34.646 mm Default Grid Snap Ortho Planar

Phoenix3D - designing structures through reuse -

members supports loads structure solver results

efficiency + reuse: design of a bus station



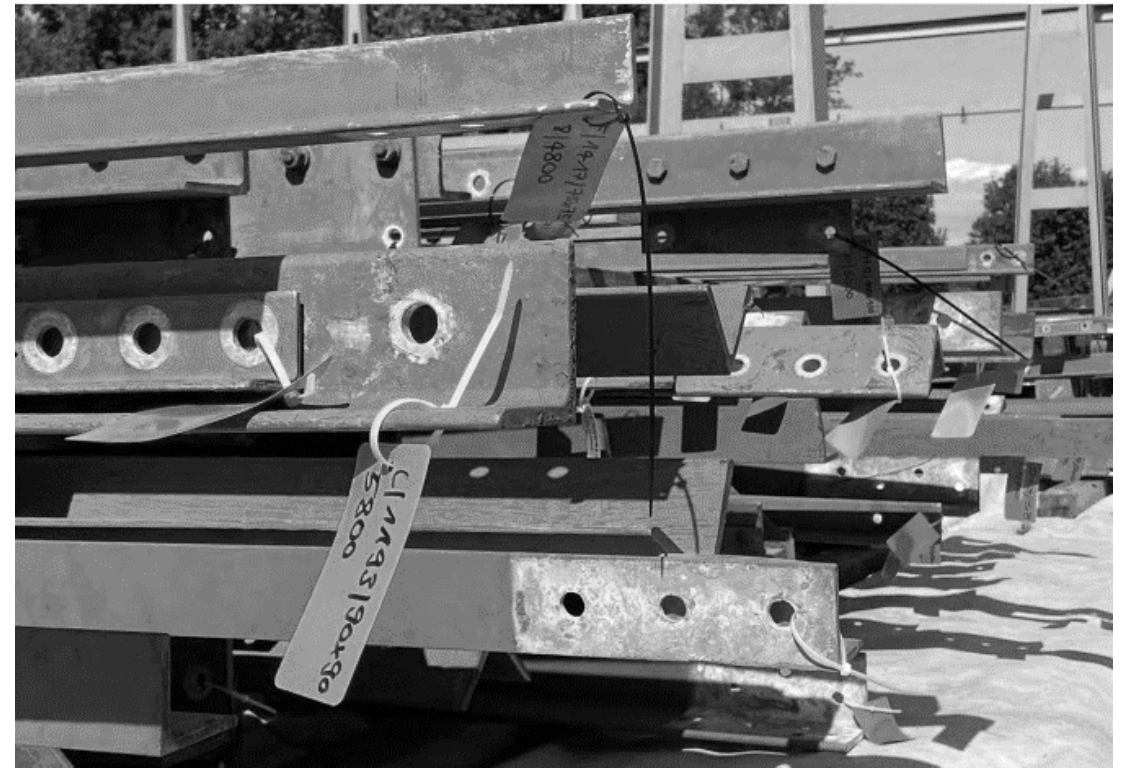
built project



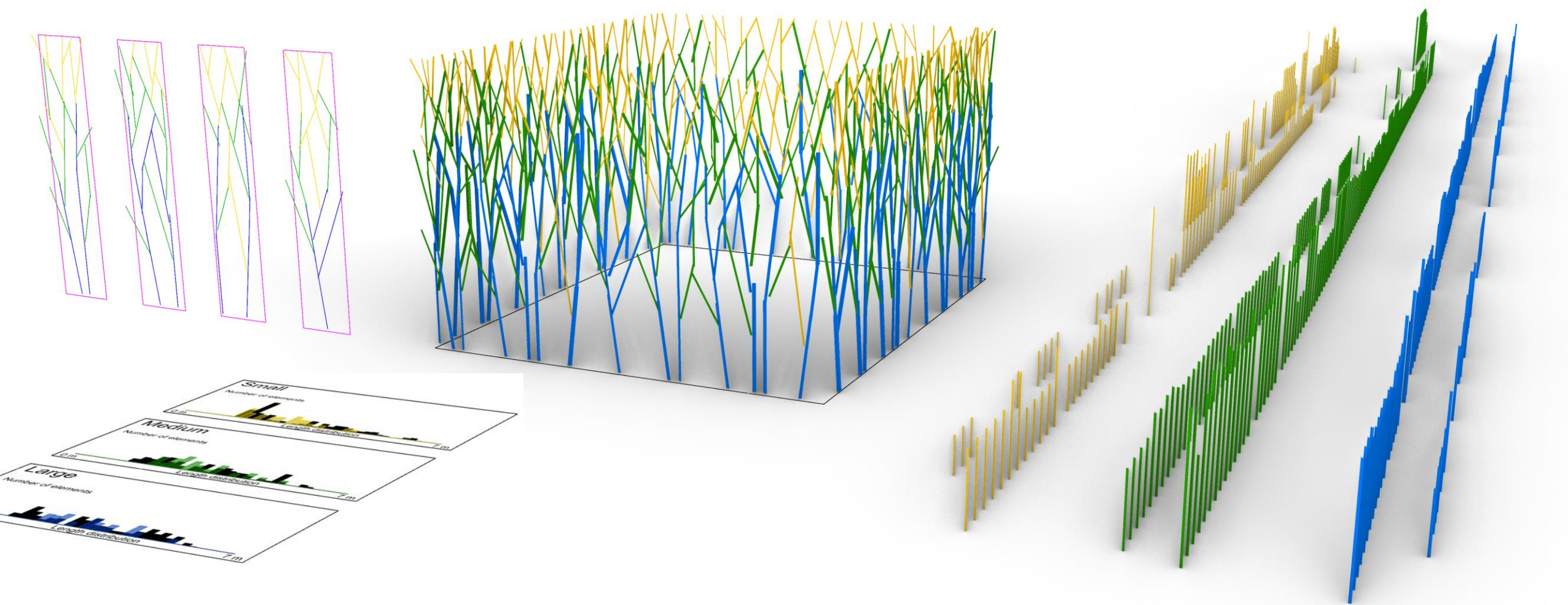
stock



swissgrid



design

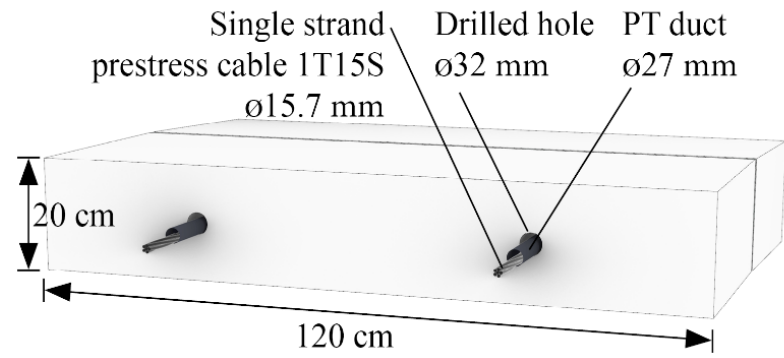




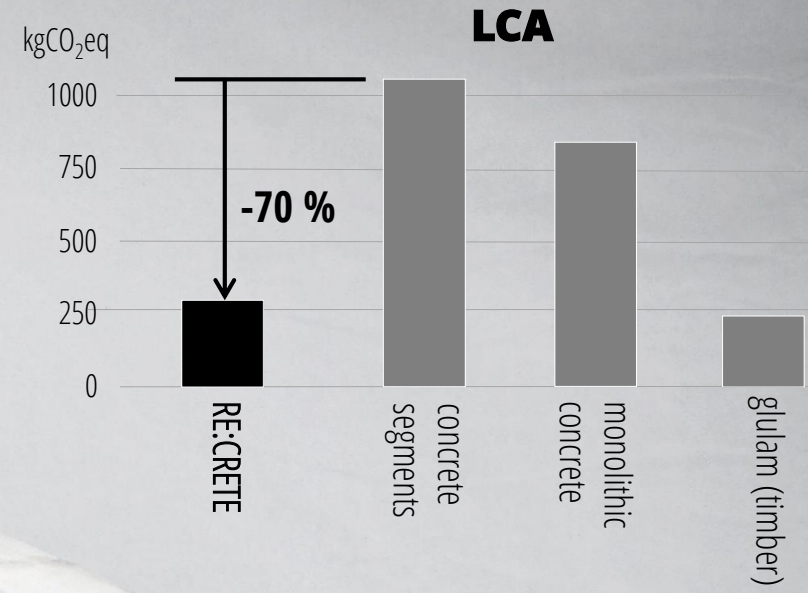
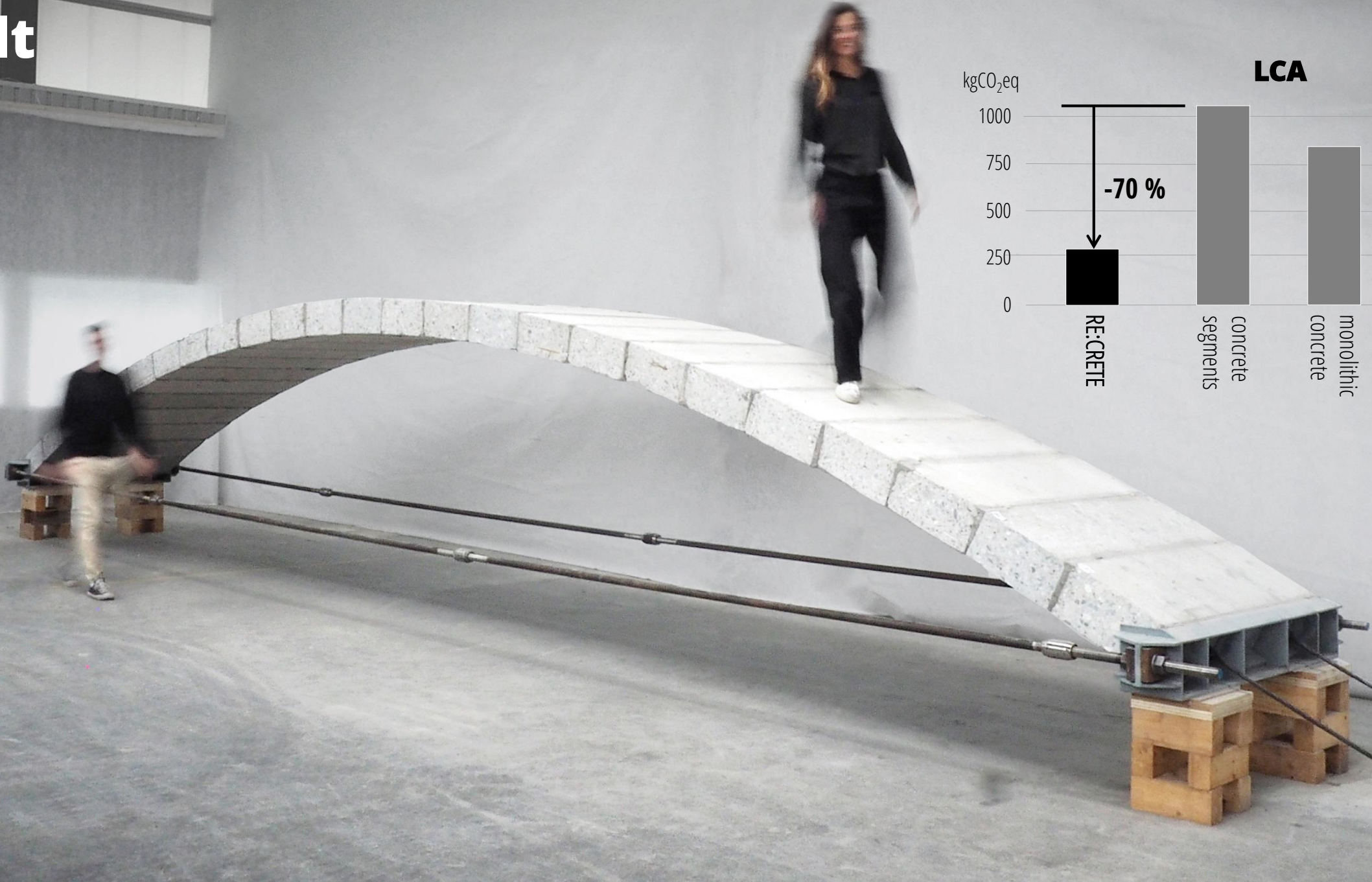




assembly



result



pre-dimensioning

pre-sizing: typical slenderness

Material	Structure	economic design l/h of a simple beam
steel	Vierendeel	7 – 10
	truss	10 - 15
	spatial truss	12 - 18
	beam	15 - 20
reinforced concrete	beam	12 - 18
	slab	20 - 25
pre-cast concrete	beam	18 - 25
	slab	28 - 35
timber	beam	15 - 20

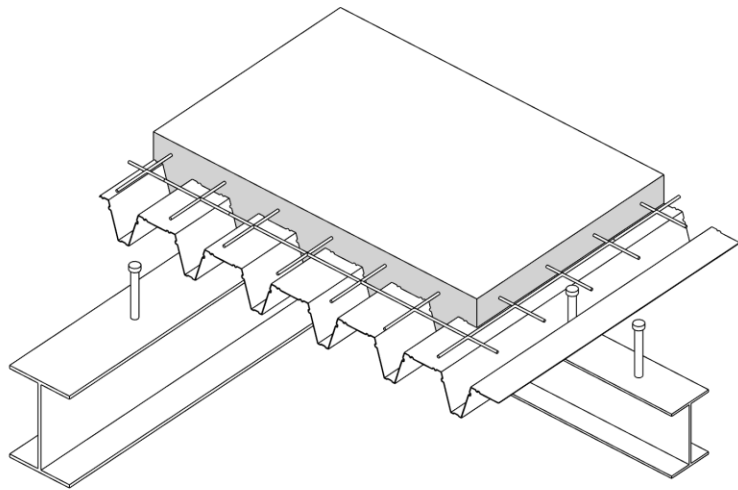
massive timber beams



glulam beams



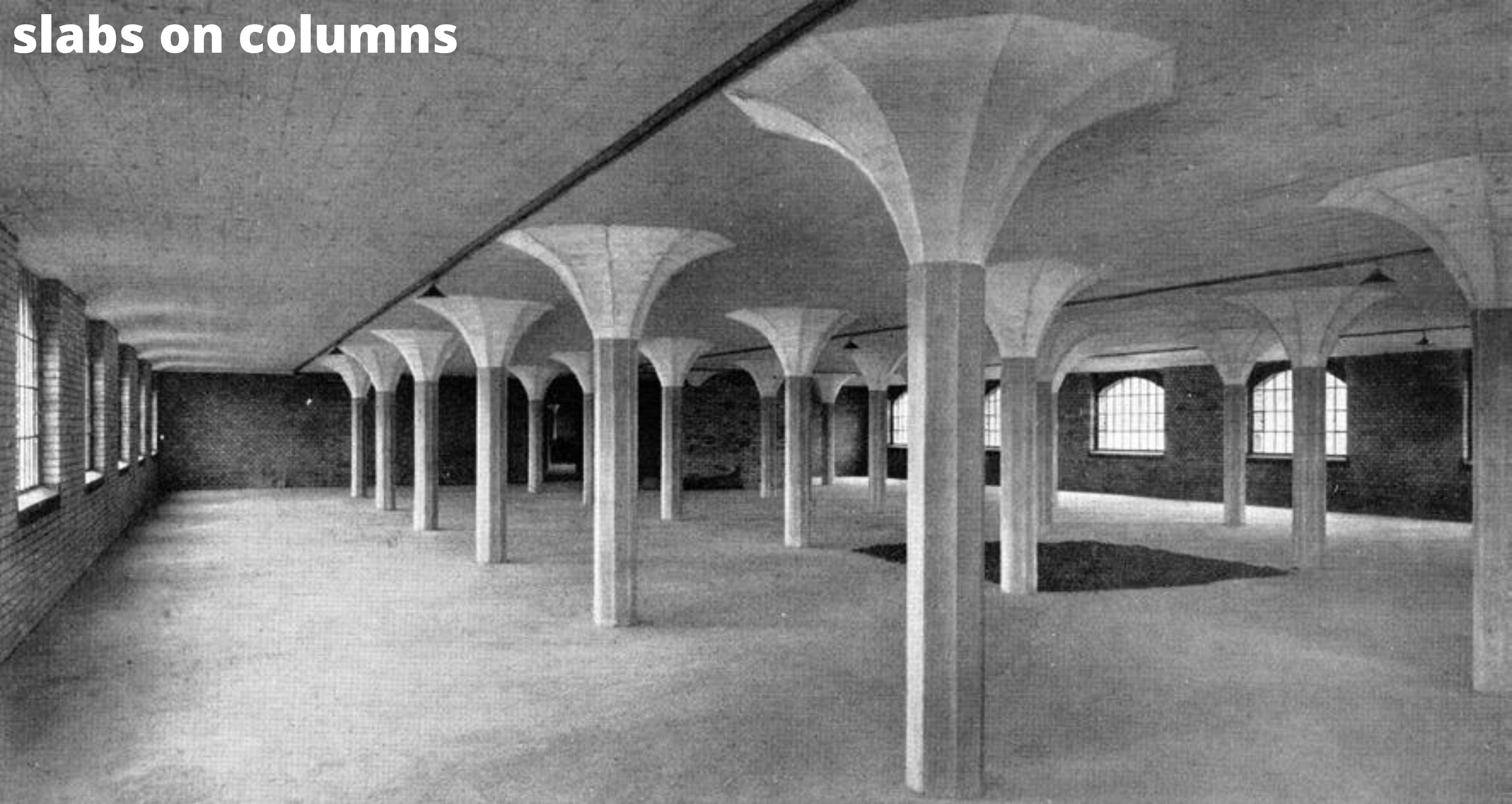
mixed floor



slabs on beams



slabs on columns



pre-sizing of reinforced concrete slabs

slab system	typical span L (economic)	recommended slenderness h/L
slab on walls	8 m	1/25 to 1/35
slab on columns	6 – 9 m	1/20 to 1/30
slab on (mushroom) columns or with additional depths	6 – 15 m	1/25 to 1/35 ($h_{\min} = 200$ mm)
slab on beams	6 – 15 m	1/25 to 1/35
ribbed slab - standard - prefabricated and pre-stressed	7 – 12 m < 18 m	Total : 1/20 to 1/35 spacing of ribs < 2h
cassette slab	12 – 20 m	ribs : 1/15 to 1/20 slab : $h_{\min} = 120$ mm
cantilevered slab	2 – 3 m	1/10

pre-sizing of columns

$$\sigma = F/A \quad [\text{N/mm}^2]$$

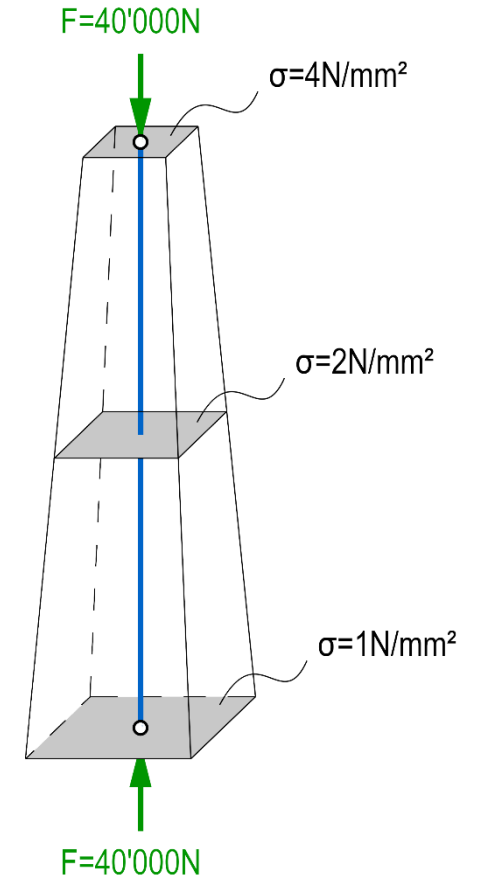
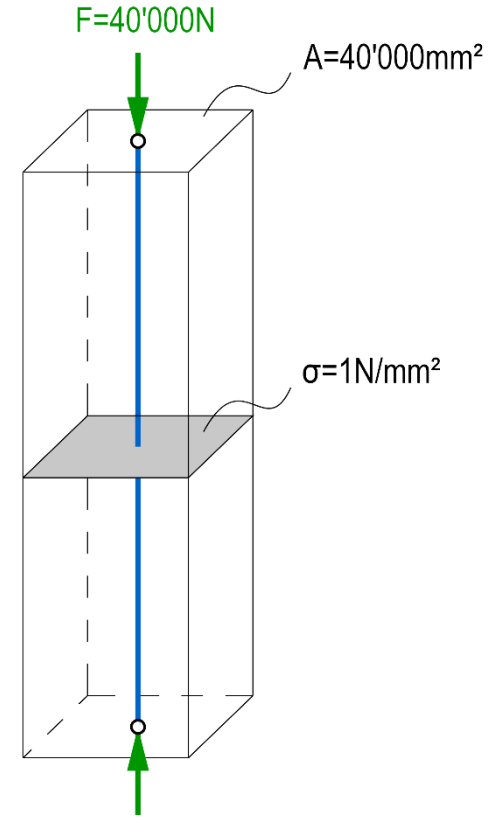
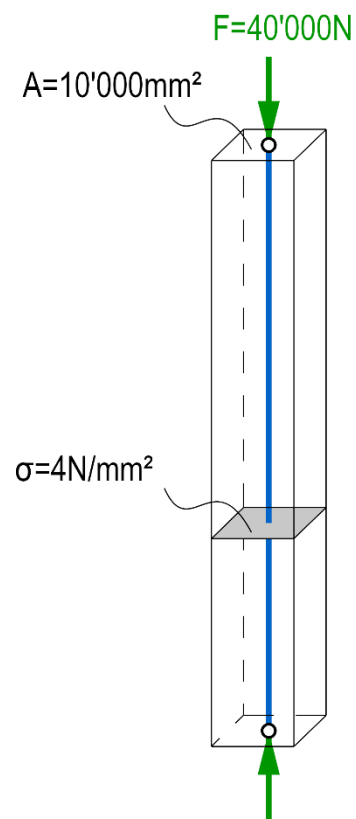
σ ("sigma") = constraint

F = axial force applied to cross-section

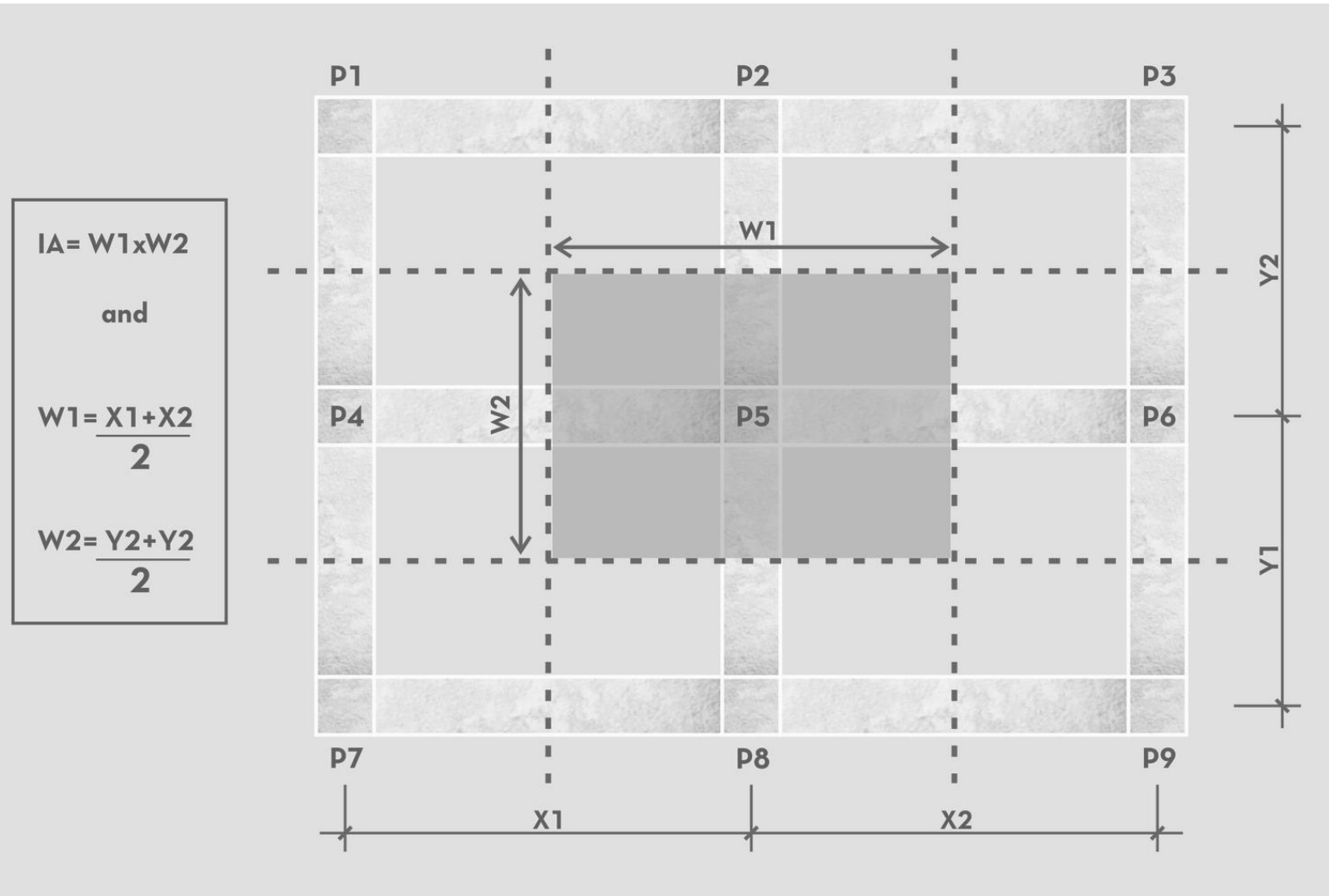
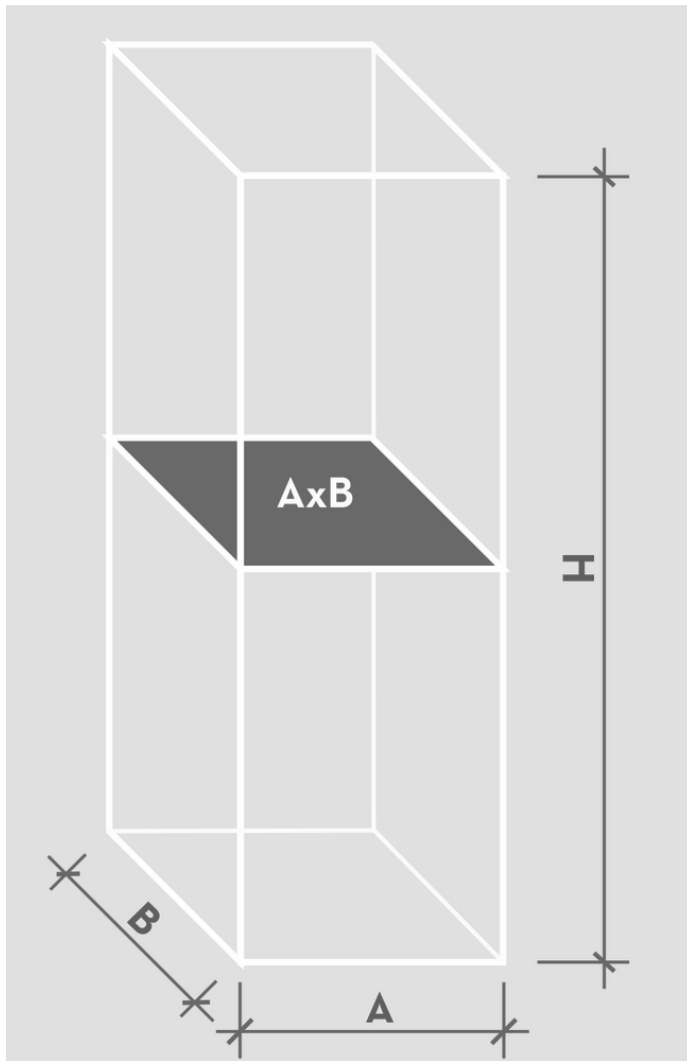
A = considered cross-section

$$1 \text{ N/mm}^2 = 1'000'000 \text{ Pa} = 1 \text{ MPa}$$

+ stability check
(buckling)



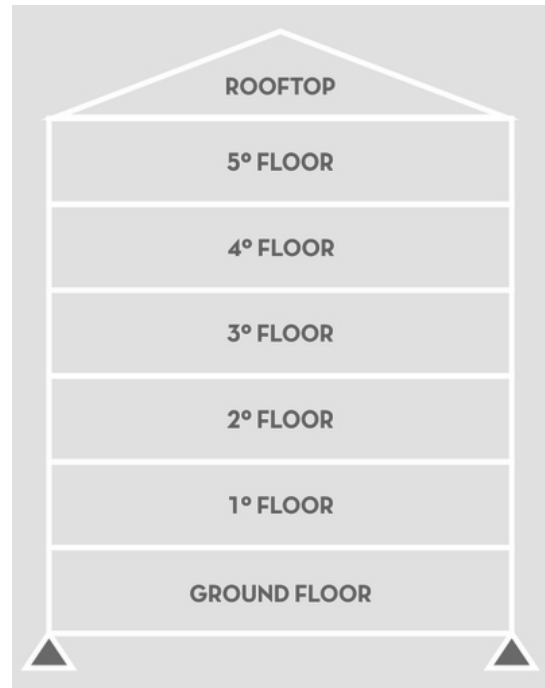
pre-dimensioning of column spacing



pre-sizing of concrete columns

assumptions:

- load
10 kN/m²
- resistance
10 MPa or N/mm²
- Min 200x200 mm



Étage	Aire d'influence	Charge	Charge accumulée	Aire poteau	Dimensions
	m ²	kN	kN	mm ²	mm
Rooftop	40	200			
5	40	400	200	20000	200x200
4	40	400	600	60000	200x300
3	40	400	1000	100000	350x350
2	40	400	1400	140000	300x500
1	40	400	1800	180000	400x500
0	40	200	2200	220000	450x450
Fondation			2400	240000	

pre-sizing of foundations

$$\text{Area foundation} = \frac{\text{load}_{\text{building}}}{\text{capacity}_{\text{sol}}}$$

$$\text{dim foundation} = \frac{\text{Area foundation}}{\# \text{ fondations}}$$

pre-sizing of foundations

$$\text{Area foundation} = \frac{\text{load}_{\text{building}}}{\text{capacity}_{\text{sol}}}$$

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Étage	Aire d'influence m ²	Charge kN	Charge accumulée kN	Aire poteau mm ²	Dimensions mm
Rooftop	40	200			
5	40	400	200	20000	200x200
4	40	400	600	60000	200x300
3	40	400	1000	100000	350x350
2	40	400	1400	140000	300x500
1	40	400	1800	180000	400x500
0	40	200	2200	220000	450x450
Fondation			2400	240000	

pre-sizing of foundations

$$\text{Area foundation} = \frac{\text{load}_{\text{building}}}{\text{capacity}_{\text{sol}}}$$

$$\text{dim foundation} = \frac{\text{Area foundation}}{\# \text{ fondations}}$$

Type of Soil	Bearing capacity kN/m2
Cohesive Soils	
Soft shale, hard or stiff clay in a deep bed, dry state	440
Medium clay readily indented with a thumbnail	245
Moist clay and Sand clay mixture which can be indented by thumb pressure	150
Black cotton soil/expansive clay (50% saturated) in dry state	130 to 160
Soft clay indented with moderate thumb pressure	100
Very soft clay which can be penetrated with the thump up to few centimetres	50
Cohesionless Soil	
Compact gravel/sand and gravel mixture with good resistance against penetration of tools	440
Compact and dry coarse sand	440
Compact and dry medium sand	245
Loose gravel or sandy gravel mixture, dry state	245
Fine sand and silt (consists of dry lumps)	150
Loose and dry fine sand	100
Rocks	
Hard rocks such as granite trap, diorite etc.	3240
Laminated rocks such as sandstone, limestone, etc.	1620
Residual deposits of shattered and broken bedrock and hard shale, cemented material	880
Soft rocks	440

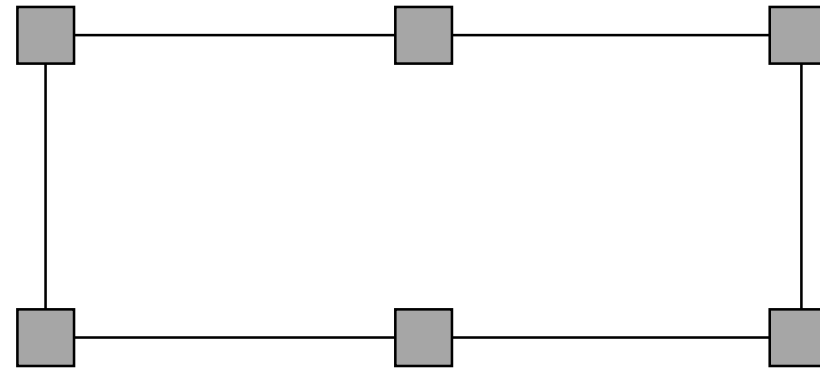
pre-sizing of foundations

$$\text{Area foundation} = \frac{\text{load}_{\text{building}}}{\text{capacity}_{\text{sol}}}$$

$$\text{dim foundation} = \frac{\text{Area foundation}}{\# \text{ foundations}}$$

$$\text{Area foundation} = \frac{2400}{440} = 5.45 \text{ m}^2$$

$$\text{dim fondation} = \frac{5.45}{6} = 0.91 \text{ m}^2 = 1 \times 1 \text{ m}$$





Structural Design & Environmental Impact

Jonas Warmuth

Dr. ès sc. – Postdoctoral researcher, Structural Engineer